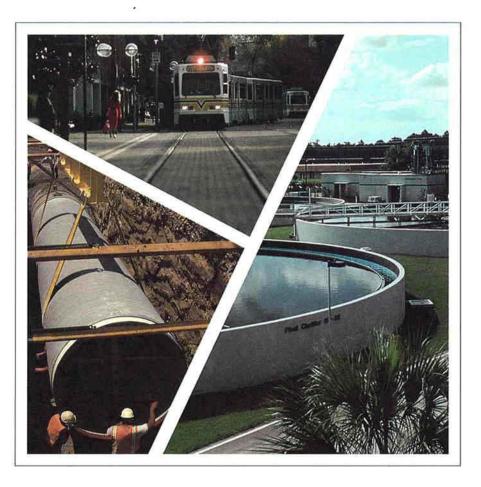
NIPOMO

COMMUNITY SERVICES DISTRICT



Water and Sewer System Master Plan FINAL REPORT



VT-N04-100-01

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NIPOMO COMMUNITY SERVICES DISTRICT

Water and Sewer System Master Plan

Nipomo Community Services District

Client Representatives

es Doug Jones, General Manager Lee Douglas, Maintenance Supervisor Lisa Souza Bognuda, Asst. Administrator

Boyle Engineering Corporation

Project Manager

Christine M. Ferrara, P.E.

Project Engineer Jeffrey A. Lodge

Quality Control

Jay T. Spurgin, PE

VT-N04-100-01

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973 Higuera St. Suite C, San Luis Obispo, CA 93401 Copy of document found at www.NoNewWipTax.com

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11-6-95

Executive Summary

In April of 1995, the Nipomo Community Services District Board of Directors authorized the preparation of this Water and Sewer System Master Plan. The purpose of this document is to identify improvements to the water distribution and wastewater collection systems to meet existing and projected demands. A facility improvement program is recommended herein, including budget guidelines and priorities associated with the recommended improvements.

Overall, the extent of deficiencies noted in the water system is average for a system of this size and age. The wastewater collection system is considered well designed to meet current needs.

Recommended Improvements to Meet Existing Needs

Water demand is projected to increase from 1,717 AFY to 2,580 AFY with an associated increase in service area population from an estimated 9,650 to 15,000.

Overall, \$3.6 million in water system improvements are recommended to reliably meet the needs of existing customers. Water System: The existing water system was found inadequate in several aspects with regard to meeting existing needs. Regarding water supply, an additional 540 gpm rate of supply is recommended to reliably meet summertime demands. Also, it was noted that the existing well pumps and motors are evidently operating at very low efficiencies. It is recommended that the District embark on a pump and motor replacement program to improve pumping efficiency and save on energy costs.

With regard to storage volume, the District currently has 2 million gallons (MG) of storage at two locations. By the criteria stated herein, an additional 1.0 MG is needed to reliably meet the needs of existing customers.

The water distribution system consists of the central business district and the outlying residential rural areas. These two areas are separated by Highway 101 and Nipomo Creek. Currently, a single 12-inch diameter waterline at Tefft Street connects these two areas. Two additional connections are recommended to improve reliability and distribution. Further, recommendations are made to connect the Black Lake water system to the main distribution system.

Other distribution system improvements are recommended to meet fire flow requirements throughout the service area, noteworthy among which is a recommendation to construct a parallel 12-inch diameter line from the Twin Tanks to the main distribution system. Overall, \$3.6 million in water system improvements are recommended to reliably meet the needs of existing customers. Note that some of the recommended improvements will be provided by developers.

Sewer System: The existing wastewater collection was found to be very well designed to handle existing needs. Two areas of note are the gravity collector in Division Street and the excess capacity of existing lift stations.

The existing wastewater collection was found to be very well designed to handle existing needs.

Regarding Division Street, an existing 8-inch diameter gravity collector transports local flow plus flow from four lift stations to the frontage road main trunk line. To address this situation, a gravity relief line which would in effect eliminate the Nipomo Palms lift station is recommended. The two existing County Service Area No. 1 lift stations could also be routed through the proposed relief line at an estimated cost of \$202,000.

Regarding the lift station capacities, it was noted that half of the District's lift stations appear over-sized to meet existing (and projected) needs. The District is advised to evaluate wet well volumes, pump and motor sizes, and on/off levels in the Bracken, North Oakglen, and Gardenia lift stations.

Recommendations for the Master Planned System

Water System: The projected 50 percent increase in water demand coupled with expansion of the service area to the west will require the installation of distribution mains, a total of 2.53 MG additional storage, and additional supplies to reliably meet projected demands. An estimated \$1.9 million in system improvements are recommended to meet projected water demands.

Wastewater flow is projected to increase from 0.35 MGD to 1.13 MGD. Sewer System: Facilities to meet projected community sewering needs include additional gravity collectors, one new lift station near Amado Street, and greater capacity in the Frontage Road trunk line. An additional \$1.5 million in sewer system improvements are recommended in addition to the Nipomo Palms lift station relief line mentioned above.

1.0 Introduction

1.1 Overview

The Nipomo Community Services District is located along Highway 101 in the southern portion of San Luis Obispo County, California, as shown on **Figure 1**. The District is situated approximately halfway between the cities of San Francisco and Los Angeles.

The District provides water and sewer service to an unincorporated area of San Luis Obispo County. Land use is regulated by the County. The District currently provides water service to approximately 9,650 people. Approximately 40 percent of the service area is currently sewered.

Nipomo has sustained a fairly brisk rate of development in recent years, a trend which is expected to continue. In order to plan for the orderly expansion of water and sewer facilities, the District selected Boyle Engineering Corporation to prepare this water and sewer system master plan. The result of this master plan is a plan for sewer collection and water distribution and storage facility upgrades to meet the needs of existing and future customers.

The District receives its supply of water exclusively from wells that pump water from the Nipomo subunit of the Santa Maria Ground Water Basin. This master plan quantifies projected water needs, but is not intended to be a water resource management planning document.

The District currently operates two separate water and sewer systems; one serving the main Nipomo area and one serving the Black Lake development. This master plan defines facilities needed to intertie the two water systems. The sewer systems are to remain separate.

Wastewater is treated and disposed at two locations, the main Nipomo wastewater treatment plant located south of the service area, and at the Black Lake development located to the northwest. Both treatment and disposal facilities are to remain in service. This master plan quantifies projected wastewater flows to both plants, but is not intended to define necessary treatment or disposal upgrades.

This master plan reflects a hydraulic planning effort, the purpose of which was not to provide extensive maps of the existing systems. The District's existing set of atlas maps are a good source of information that clearly shows the layout of the existing systems.

1.2 Purpose and Scope

The purpose of this study is to identify improvements to the sewer collection and water distribution systems required to meet existing and projected demands, and to develop a sewer and water facilities improvement program to aid the District in conducting long-term planning. Specific tasks which were undertaken to accomplish this include:

a. Collection and Review of Data Water data was collected which included distribution system record drawings, water consumption records, water production records, well and storage characteristics, land use plans and topographic mapping.

Sewer data was collected which included records of existing collector diameter, slope, and manhole locations throughout the service area. Additionally, information was reviewed on lift stations, including wet well depth and volume, number and type of pumps in place, and force main diameter and location.

Population and land use information was obtained from the County of San Luis Obispo Department of Planning and Building. District water usage records were also referenced to estimate the number of water service connections in recent years.

b. Development of Design Parameters Water duty factors for both residential and non-residential land uses were developed using historic water consumption data. Peaking factors for maximum day demand and peak hour demand were estimated. Fire flow requirements were established by comparison with water systems of similar complexity, climate and population.

Sewer duty factors for both residential and non-residential land uses were developed using a ratio of historic water consumption data.

c. Estimated Demands Existing land use information obtained from the San Luis Obispo County Department of Planning and Building, along with District records, were used to approximate existing and future demand distribution. Existing and future sewer loading was based on similar available information. d. Development of Computer Models Computer models were developed to simulate the District's sewer and water system performance under both existing and future demands. The District's sewer and water systems were reviewed through as-built and record drawings. Data input files were compiled for use with hydraulic and sewer network software, BoyleNET and BoyleSWAN.

The water model was calibrated using results of fire hydrant flow tests performed by District staff.

e. Identification of Existing Deficiencies and Future Needs Hydraulic analyses were performed to analyze the adequacy of the existing sewage collection and water distribution pipelines under both existing and projected demands. Upgrades were recommended where deficiencies were found. Recommendations for existing and future lift stations, conveyance systems, and storage facilities were made.

f. Prioritization and Cost Estimation for Recommended Improvements The cost and priority of recommended improvements to meet existing and projected water and sewer demands were established and a capital improvement plan was prepared.

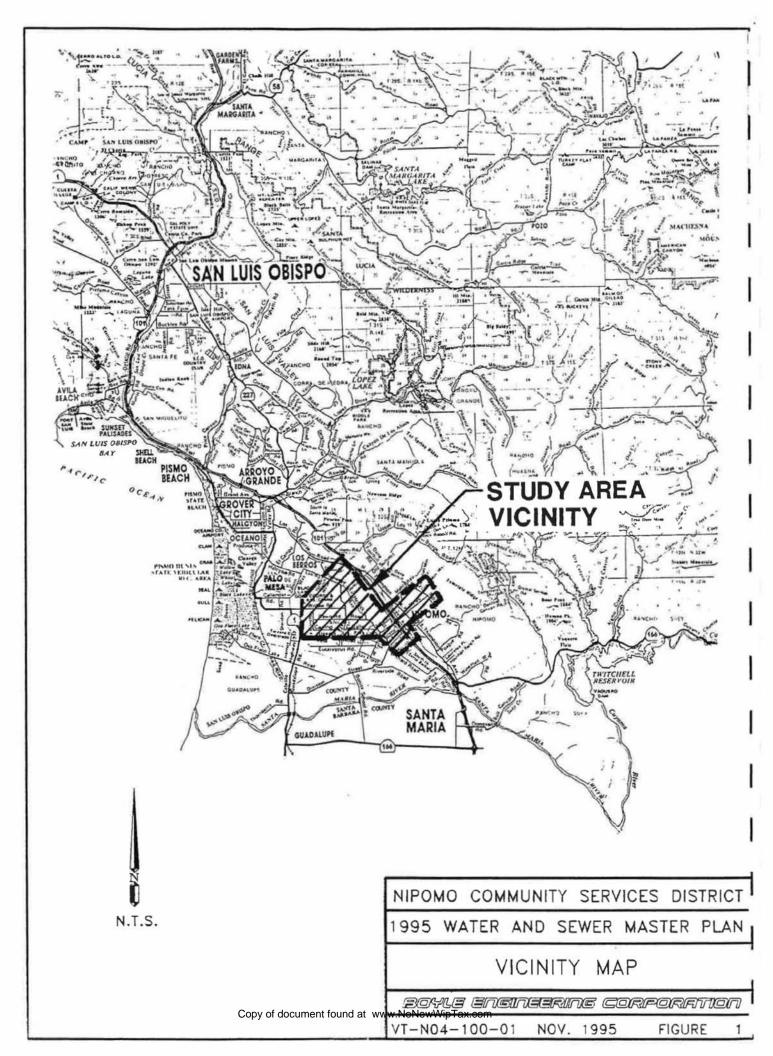
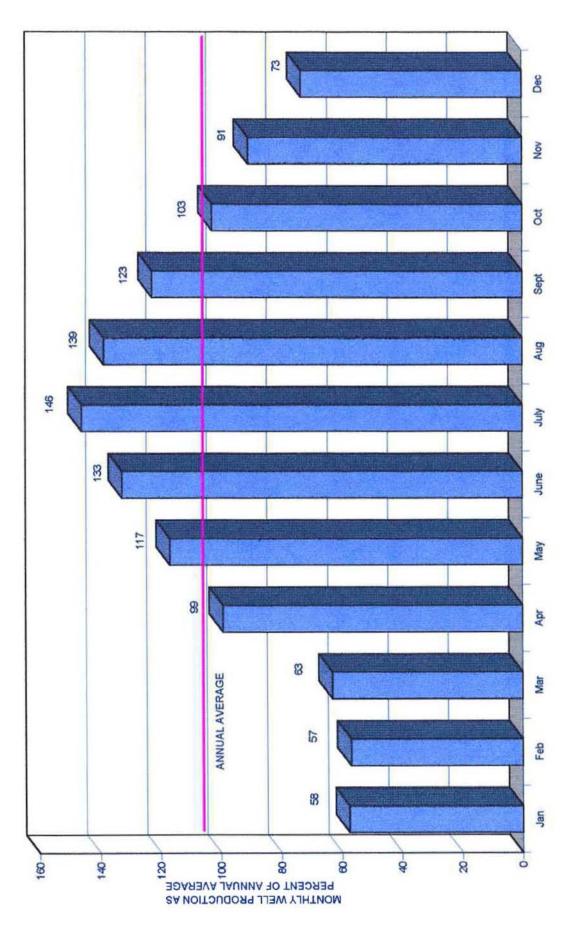
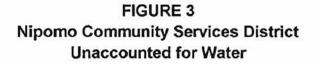
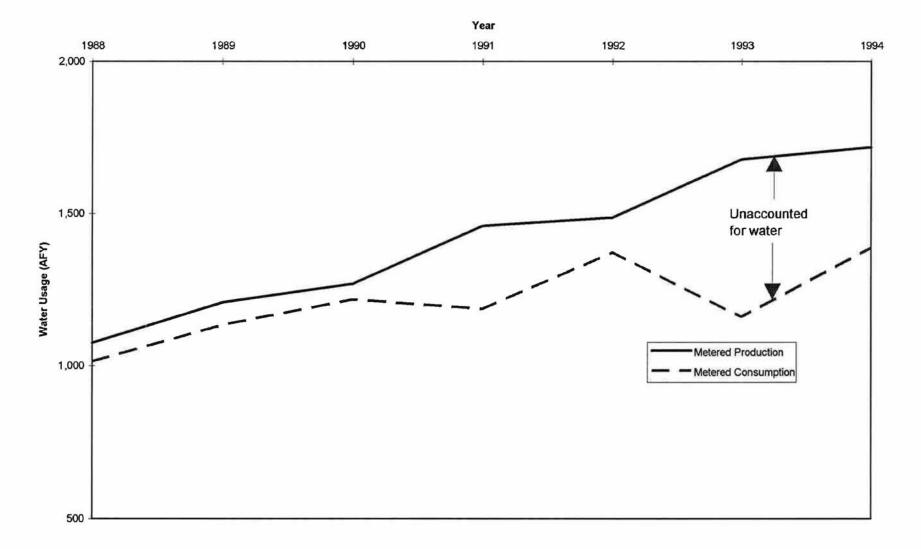


FIGURE 2 AVERAGE MONTHLY WELL PRODUCTION For Years 1988 - 1994



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2.0 Water Demands and Sewer Loading

2.1 Historic Demand

Historic water production and metered consumption data for January 1988 to March 1995 was obtained from District staff. This data is included in **Appendix A**. Water production represents the total metered production from each of the District's wells. Consumption, on the other hand, represents the sum of all metered water sales throughout the service area. From this data, average annual and peak monthly water demands were estimated.

Current average annual water demand is estimated to be 1,717 acrefeet per year (AFY) based on 1993/94 production records. Peak monthly production is estimated to be 220 AF. These estimates include both the main Nipomo system as well as the Black Lake development.

Water demand increases during the hot Summer months as illustrated in **Figure 2**. Typically, summertime demand is up to 1.5 times higher than average annual demand. The peak monthly water demand was July 1994 at which time monthly water use was 1.52 times average annual demand.

The District provided records of treated wastewater volumes at the main treatment plant for 1993 to 1995, with the explanation that some operational problems have plagued the meter. Temporary flow metering information was not made available during the course of this master plan development. Therefore, sewage flows were estimated based on both metered water production and available records of treated wastewater as described in Section 2.3.

2.2 Unaccounted For Water

Both water production and consumption records for the 1988 to 1995 period were reviewed. The difference between metered water production and metered water consumption is known as "unaccounted for water." There is typically unaccounted for water in every domestic water system, comprised of:

- Distribution system and lateral leakage
- Metering inaccuracies
- Hydrant flows
- Unmetered connections to the system

Other factors

For Nipomo, unaccounted for water has ranged from 4 to 31 percent in the past seven years, as shown in Figure 3. Unaccounted for water is typically 15 percent for systems of this size, as discussed in AWWA Manual M32.

Nipomo sustained an average unaccounted for water level of approximately 8 percent from 1988 to 1993, which is considered fair for a system of this size. Significant increases since 1992 may be attributed to widespread failure of service laterals. The District is actively replacing service laterals and is demonstrating a favorable decrease in the amount of unaccounted for water.

2.3 Determination of Water and Sewer Duty Factors

Water Duty Factors

The District's monthly water production and consumption records (Appendix A) were used as the basis for estimating water "duty factors." Duty factors are estimates of water demand per residence or per land use category.

The District provided Assessor's Parcel Maps which indicated individual lots receiving water and/or sewer service. This provided both an accurate count of the number of lots receiving service as well as a basis for distributing water demand throughout the service area. Metered consumption data for large users was also provided and was considered in estimating water duty factors for Nipomo.

First, overall water production was compared to estimates of current service area population. Statistics for the South County Planning Area, as published by the County of San Luis Obispo, were referenced. Current water service area population is estimated to be 9,650 based on estimated occupancy rates indicated in **Table 1**. This equates to a gross per capita consumption rate of 160 gallons per capita per day. "Gross" per capita consumption refers to total community water demand, including non-residential water uses.

The District provides water service to businesses, schools, irrigation meters, and other land uses in addition to residences. To estimate the water demand associated with non-residential land uses, water consumption records for specific users were referenced. Acreages for non-residential users were also estimated based on the Assessor's Parcel Maps provided by the District.

Table 1 indicates the estimated number of residential dwelling units inboth the main and Black Lake systems. Similarly, non-residential landuses are also tabulated. Average annual and "summertime demands"(i.e. May through August) are both listed in Table 1.

Sewer Duty Factors

As was previously mentioned, the District maintains records of sewage flow at the main wastewater treatment plant, however, the accuracy of the metered data is questionnable due to reported operational problems with the flow meter. Records indicate that:

- Average monthly flow in 1993 was measured at 0.228 MGD
- Average monthly flow in 1994 was measured at 0.273 MGD
- Average monthly flow for the first eight months of 1995 was measured at 0.31 MGD

Metered flow data for the Black Lake wastewater treatment plant is not available.

The District currently operates eight sewage lift stations. Records of monthly electrical use is available at each lift station, however, accurate records of pump capacity are not. The District asked PG&E to conduct pump efficiency tests at each lift station earlier this year, however, PG&E declined to use their flow measurement device on wastewater facilities.

It was determined that the best available data upon which to estimate sewage loading duty factors was water consumption data. Estimates of the ratio of water use that flows to the sewage collection system were made for each land use category. This was compared to available metered flow data for the main treatment plant.

The number of residential units and non-residential development within each of the seven lift station tributary areas were estimated based on the District's Assessor's Parcel Map information. These are tabulated in **Table 2**. Nominal lift station capacities were compared to PG&E records to estimate the average flows handled at each lift station. Estimates of sewer duty factors were iteratively derived to arrive at the sewage duty factors listed in **Table 2**.

Using this method, average annual flows to the main Nipomo wastewater treatment plant are estimated to be 0.35 MGD. This compares to meter records indicating a 0.31 MGD average monthly flow rate for the first eight months of 1995. The Black Lake treatment plant is estimated to treat an average of 69,000 gpd.

It should be noted that the District's sewage collection system handles sanitary flows only. A separate storm drain system is maintained by the County.

TABLE 1 WATER DUTY FACTORS USED FOR EXISTING SYSTEM ASSESSMENT

MAIN NIPOMO WATER SYSTEM:

User	Est. No. of Units (dwelling units) (1)	Est. Occupancy Rate (persons/unit)	Est. per Capita Consumption (gpcd) (2)	Avg. Annual Demand (gpd) (3)	Summertime Demand (gpd) (3)
Residential Unit - Large Lots	690	4.50	120	372,600	469,500
Residential Unit - Small Lots	1,086	3.50	93	353,500	445,400
Residential Multi-Family	999	2.10	89	186,800	235,400
RESIDENTIAL SUBTOTAL =	2,775			912,900	1,150,300
EST. MAIN SERVICE AREA P	OPULATION =	9,005			a 8
	Est. No. of Acres (acres)		Est. Consumptio Rate (gal/acre/day)	Avg. Annual Demand (gpd) (3)	Summertime Demand (gpd) (3)
Commercial Service Acreage	30	N/A	1.000	30,300	38,200
Commercial Retail Acreage	152	N/A	1,200	182,300	229,700
Office/Professional Acreage	34	N/A	900	31,000	39,100
Public Facility Acreage	9	N/A	2,200	19,400	24,400
NON-RESID. SUBTOTAL =	226			263,000	331,400
Large Users:					
Nipomo Regional Park				34,400	64,630
Nursery-675 Grande				13,240	17,180
Bar K Mobile Home Park				12,840	16,170
Vons Mobile Home Park				5,720	9,230
Nipomo Recreation Assoc				5,140	8,880
Church-312 Oakglen				4,380	4,510
Swap Meet				4,150	5,430
Buena Vista Mobile Homes				3,880	5,400
Landscape mtr-479 Socios				3,560	5,530
Laundromat-277 Tefft				3,310	4,000
Jockos Restaurant				3,290	3,430
9 units-475 Amado	2			2,850	3,660
Commercial-Frontage/Sandyda	ale			2,660	3,760
Bank of Santa Maria				2,440	3,520
St. Joseph's Church				2,120	2,510
Grande Apts Landscape Meter				1,830	2,670
Miscellaneous Irrigation Meters	s			21,480	21,480
LARGE USER SUBTOTAL =				127,290	181,990
TOTAL WATER DEMAND					
MAIN NIPOMO WATER SYST	TEM =			1,303,190 gpd 905 gpm	1,663,690 gpd 1,155
BLACK LAKE WATER SY	STEM:			1,460 AFY	

User	Est. No. of Units (dwelling units) (1)	Est. Occupancy Rate (persons/unit)	Est. per Capita Consumption (gpcd) (2)	Avg. Annuai Demand (gpd) (3)	Summertime Demand (gpd) (4)	
Black Lake Residences	321	2.00	245	157,100	223,750	
Black Lake Irrigation Usage	N/A	N/A	N/A	73,300	87.250	
TOTAL BLACK LAKE WATE	R DEMAND =			230,400	311,000	
EST. BLACK LAKE POPULAT	TION =	642		gpd 160 gpm 258 AFY	gpd 216	
TOTAL EST. SERVICE AREA	POPULATION =	9,647				

Source: Assessor's Parcel Maps provided by District and 1994 Public Water System Statistics.
 Est. per capita and non-residential consumption based on metered production data and occupancy rate data provided by District.
 Average annual and summertime (May to August)water production data from well production records provided by the District. Average annual demand = no. of units x occupancy x consumption rate.

TABLE 2 SEWER DUTY FACTORS AND EXISTING FLOWS

% of Water		Water Use apd. or	Sewer Flow at	
Going to Sewer		gpd/acre	% stated	
0.55	Res. Lg. lot	540	297	gpd/lol
0.6	Res. Sm lot	325	195	gpd/lot
0.8	Comm. Retail	1200	960	gpd/acre
0.9	Comm. Service	1000	800	gpd/acre
	Office/Prof.	900	720	gpd/acre
	Public Facility	2200	1760	gpd/acre
	Resid. Multi Family	1870	1683	gpd/acre
	0.55 0.6 0.8	Going to Sewer Res. Lg. lot 0.55 Res. Sm lot 0.6 Res. Sm lot 0.8 Comm. Retail 0.9 Comm. Service Office/Prof. Public Facility	% of Watergpd, orGoing to Sewergpd/acre0.55Res. Lg. lot0.6Res. Sm lot0.8Comm. Retail0.9Comm. Service000Office/Prof.900Public Facility2200	% of Water gpd, or gpd/acre Flow at % stated 0.55 Res. Lg. lot 540 297 0.6 Res. Sm lot 325 195 0.8 Comm. Retail 1200 960 0.9 Comm. Service 1000 800 Office/Prof. 900 720 1760

MAIN NIPOMO SEWER SYSTEM:

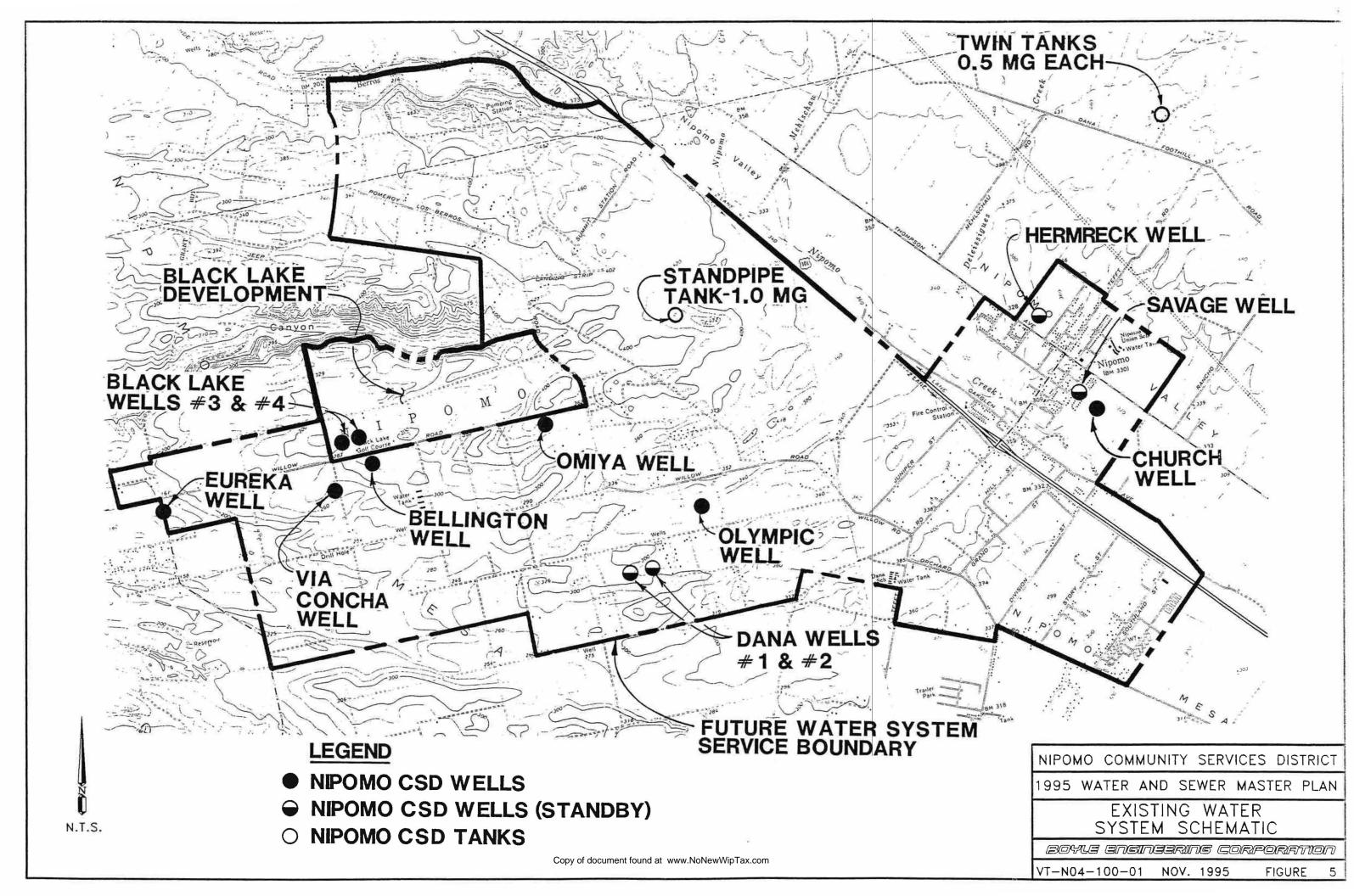
TRIBUTARY AREA	NO. OF LARGE LOTS	NO. OF SMALL LOTS	Commercial Retail (acres)	Commercial Service (acres)	Office/ Professional (acres)	Public Facility (acres)	RMF (acres)	Est. Flow (gpd) (1)	Flow based on run time (gpd) (2)	Diff. (3)
Tefft Street Lift Station	1	368	5.06	0	1.77	6.93	16.98	118,963	129,464	8%
Black Lake Mobile Home Park LS	0	156	0	0	0	0	0	30,420	27,615	-10%
Bracken Lift Station	o	16	o	0	0	0	٥	3,120	2,772	-13%
Gardenia Way Lift Station	0	21	0	0	0	0	0	4,095	2,198	-86%
North Oakglen Lift Station	1	18	o	0	٥	1.89	0	7,133	7,350	3%
La Mirada Lift Station	0	83	٥	0	O	0	0	16,185	13,224	-22%
Vipomo Palms Lift Station	0	92	5.1	0	0	0	0	22,836	20,580	-11%
Gravity flow to Treatment Plant	23	121	21.97	0	0	0	7.66	64,409	64,409	N/A
CSA-1 (4) Galaxy Park People's Self Help Lift Station	: 							53,382 24,570	53,382 24,570	N/A N/A
Totals	25	875	32.13	0.00	1.77	8.82	24.64	345,114	345,564	
								0.35 MGD	0.35 MGD	

(1) Estimated flow is average dry weather flow based upon number of tributary residential units at the sewer duty factors stated above and based upon the approximate number of acres of non-residential land use at the sewer duty factors stated above.

(2) Tributary area flow based on lift station run time is the total number of hours of operation for each lift station per month during January thru June 1994 times the nominal lift station flow capacity for each station.

(3) "Difference" is the percentage difference between calculated tributary area flow based on duty factors as compared to actual run time records for 1994. The large difference associated with Gardenia Way lift station represents a relatively small difference in average flow.

(4) Galaxy Park and Peoples Self Help Housing lift station flow estimates based on nominal lift station capacity times estimated station run time.



2.4 Projected Demand

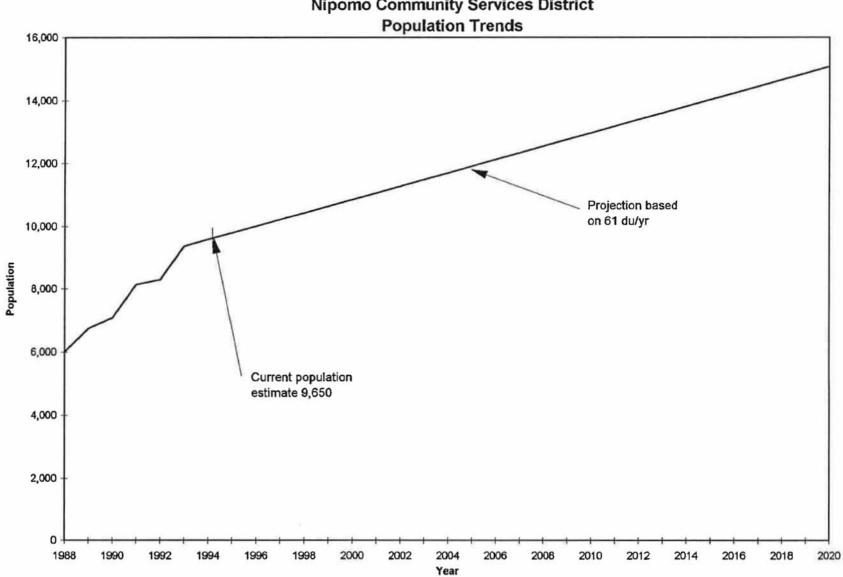
This master plan is based on extending water and sewer service to the future service area boundaries illustrated in **Figures 5 and 6** respectively. Water service area population trends are illustrated in **Figure 4**. From 1988 to 1994, approximately 200 new connections per year have been added to the water system. Many factors affect the pace at which development will continue within Nipomo. **Figure 4** population projections are based on a sustained building rate of approximately 61 residential units per year. At this rate, the projected ultimate service area population of 15,000 would be reached in the year 2020.

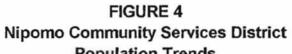
The County Land Use Element and Local Coastal Plan was referenced to determine land use zoning within the service area boundaries. Future areas to be served were tabulated in terms of additional residential units and non-residential land use acreages. The water and sewer duty factors shown in **Tables 1 and 2** were used to estimate water demands and sewage loadings within the study area. Areas currently zoned agriculture are presumed to be converted to residential zoning for the purposes of projecting water and sewer needs.

Projected water demand is summarized in Table 3.

Based on the total number of acres for residential land uses along with occupancy rates as shown in **Table 1**, projected water demand is estimated to be 2,580 AFY. The distribution pipelines proposed in this master plan have been sized and laid out to accommodate this projected water usage.

Regarding sewer needs, **Table 4** tabulates the projected sewage loading throughout the service area illustrated in **Figure 6**. At full build-out and at 100% occupancy, average annual wastewater flows to the main Nipomo wastewater treatment plant are projected to be 1.13 MGD. Average annual flows to the Black Lake plant are projected to be 120,000 gpd based on 553 occupied units.





wateruse.xls

TABLE 3 FUTURE LAND USE AND WATER DEMAND

MAIN NIPOMO WATER SYSTEM:

User	Est. No. of Units (dwelling units) (1)	Est. Occupancy Rate (persons/unit)	Est. per Capita Consumption (gpcd) (2)	Avg. Annual Demand (gpd) (3)	Summertime Demand (gpd) (3)
Residential Unit - Large Lots	1,405	4.50	120	758,700	956,000
Residential Unit - Small Lots	1,469	3.50	93	478,100	602,400
Residential Multi-Family	1,197	2.10	89	223,800	282,000
RESIDENTIAL SUBTOTAL =	4,071			1,460,600	1,840,400
EST. MAIN SERVICE AREA POP	PULATION =	13,978			
	Est. No. of Acres		Est. Consumption Rate	Avg. Annual Demand	Summertime Demand
	(acres)		(gal/acre/day)	(gpd) (3)	(gpd) (3)
Commercial Service Acreage	82	N/A	1,000	81,900	103,200
Commercial Retail Acreage	199	N/A	1,200	239,400	301,600
Office/Professional Acreage	36	N/A	900	32,600	41,100
Public Facility Acreage	9	N/A	2,200	19,400	24,400
NON-RESID. SUBTOTAL =	326			373,300	470,300
Large Users:					
Nipomo Regional Park				34,400	64,630
Nursery-675 Grande				13,240	17,180
Bar K Mobile Home Park				12,840	16,170
Vons Mobile Home Park				5,720	9,230
Nipomo Recreation Assoc				5,140	8,880
Church-312 Oakglen				4,380	4,510
Swap Meet				4,150	5,430
Buena Vista Mobile Homes				3,880	5,400
andscape mtr-479 Socios				3,560	5,530
aundromat-277 Tefft				3,310	4,000
Jockos Restaurant				3,290	3,430
9 units-475 Amado				2,850	3,660
Commercial-Frontage/Sandydale				2,660	3,760
Bank of Santa Maria				2,440	3,520
St. Joseph's Church				2,120	2,510
Grande Apts Landscape Meter				1,830	2,670
Miscellaneous Irrigation Meters				21,480	21,480
LARGE USER SUBTOTAL =				127,290	181,990
TOTAL WATER DEMAND					
MAIN NIPOMO WATER SYSTE	M =			1,961,190	2,492,690
				gpd	gpd
				1,362 gpm 2,197 AFY	1,731 gp

BLACK LAKE WATER SYSTEM:

User	Est. No. of Units (dwelling units) (1)	Est. Occupancy Rate (persons/unit)	Est. per Capita Consumption (gpcd) (2)	Avg. Annual Demand (gpd) (3)	Summertime Demand (gpd) (4)
Black Lake Residences	553	2.00	245	270,970	401,036
Black Lake Irrigation Usage	N/A	N/A	N/A	73,300	87,250
TOTAL BLACK LAKE WATER	R DEMAND =	1111 A.		344,270	488,286
EST. BLACK LAKE POPULAT	TON =	1,106		gpd 239 gpm 386 AFY	дрd 339 дрп
COMBINED SYSTEMS:	Population			Avg. Annual Demand	Summertime Average
	15,084			2,582 AFY	2,070 gpm

Source: Exist. no. of units (Table 1) plus infill in developed areas and zoning as defined by SLO County in undeveloped areas.
 Per capita consumption estimated to remain at existing levels.
 Average annual estimated at duty factors stated above. Summertime (May to August) demand estimated to be 1.27 times average annual demand; 1.48 for Black Lake.

TABLE 4 PROJECTED SEWAGE LOADING

Land Use	% of Water Going to Sewer		Water Use gpd, or g <u>pd/acre</u>	Sewer Flow at <u>% stated</u>	
Res-Lg lot	55%	Res. Lg. lot	540	297	gpd/lot
Res-Sm lot	60%	Res. Sm lot	325	195	gpd/lot
All acreages	80%	Comm, retail	1200	960	gpd/acre
RMF	90%	Comm, Service	1000	800	gpd/acre
		Office/Prof.	900	720	gpd/acre
		Public Facility	2200	1760	gpd/acre
		Resid. Multi Family	1870	1683	gpd/acre

MAIN NIPOMO SEWER SYSTEM:

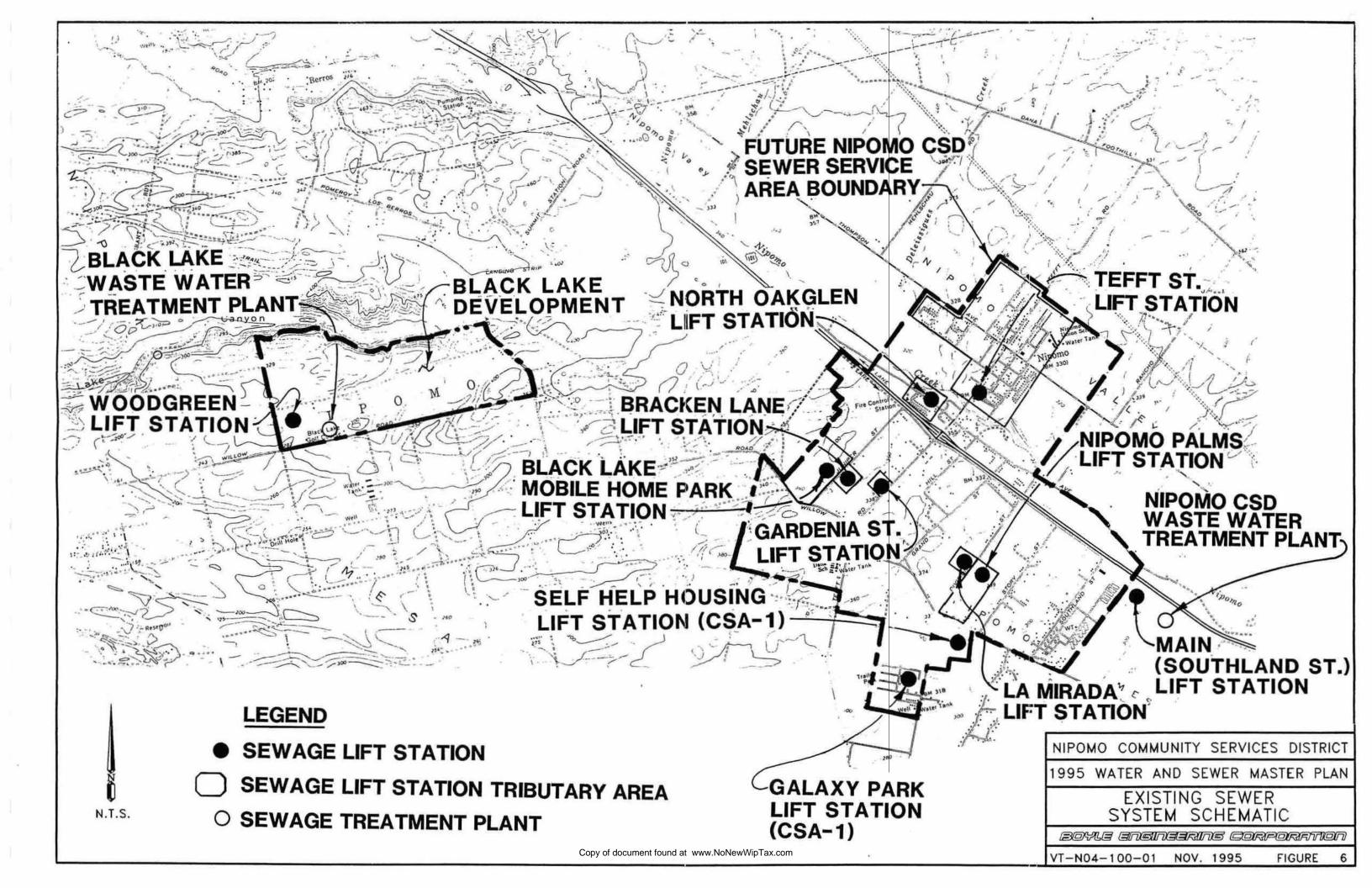
TRIBUTARY AREA	NO. OF LARGE LOTS	NO. OF SMALL LOTS	Commercial Retail (acres)	Commercial Service (acres)	Office/ Professional (acres)	Public Facility (acres)	Resid. Multi Fam (acres)	Est. Flow (gpd) (1)
Tefft Street Lift Station	23	625	47.74	o	12.4	12.55	24.63	247,005
Black Lake Mobile Home Park LS	12	156	0	0	0	0	0	33,984
Bracken Lift Station	19	18	0	0	0	0	0	9,153
Gardenia Way Lift Station	19	24	0	0	6.7	0	0	15,147
North Oakglen Lift Station	39	32	o	15.67	11.84	1.89	o	42,210
a Mirada Lift Station	0	83	0	0	0	0	0	16,185
Nipomo Palms Lift Station	0	92	5.1	0	0	0	o	22,836
Gravity flow to Treatment Plant	357	637	93.97	55	0	0	98.66	530,500
Proposed Amado Street LS	0	229	0	0	0	0	0	44,655
CSA-1								
Galaxy Park (2)	50	275	5	0	0	10	0	144,257
People's Self Help Lift Station			2 - 2	-	()	(🖃	-	24,570
Future Totals	519	2171	152	71	31	24	123	1,130,502

1.13 MGD

(1) Estimated flow is average dry weather flow based upon number of tributary residential units at the sewer duty factors stated above and based upon the approximate number of acres of non-residential land use at the sewer duty factors stated above.

(2) Galaxy Park flows include new development listed above plus existing lift station flows.

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2.5 Fire Flow Requirements

It is often the case that meeting fire flow requirements governs the sizing of a community's water distribution system. Thus, it is important to establish realistic fire flow requirements for both existing and future development. The California Department of Forestry provides fire protection services to Nipomo. CDF was contacted for information regarding fire flow requirements throughout Nipomo. CDF reportedly uses the Uniform Fire Code and the Insurance Services Organization guidelines to establish flow requirements.

ISO guidelines state recommended flows based on such factors as structure size, construction type, proximity to adjacent structures, storage of combustible materials, and other factors. Neither ISO guidelines nor CDF records are reduced to specific flow requirements per land use categories.

Planning the water system, however, requires establishment of fire protection guidelines throughout the service area. To establish such planning guidelines for Nipomo, fire flow criteria for neighboring communities was referenced.

Table 5 summarizes recommended fire flow requirements for various types of developments. Water system improvements proposed herein are based on meeting a 1,000 gpm residential fire demand at a minimum residual pressure of 20 psi. Similarly, the system's ability to meet a 3,000 gpm commercial and public facility fire demand at 20 psi minimum pressure was assessed.

TABLE 5 FIRE FLOW CRITERIA						
ZONING	REQ. FLOW AT 20 PSI MINIMUM PRESSURE (gpm)	DURATION (hours)	NUMBER OF HYDRANTS FLOWING			
Residential Rural	1,000	2	1			
Residential Suburban	1,000	2	1			
Res. Single Family	1,000	2	1			
Summit Station	1,000	2	1			
Res. Multiple Family	1,500	2	1			
Commercial Retail	3,000	3	2			
Commercial Service	3,000	3	2			
Office & Professional	1,500	2	1			
Public Facility	3,000	3	2			

2.6 Peaking Factors

Water

In the preceding sections, water demand and sewage loading were described principally in terms of average annual flows. However, both water demand and sewage flow rates vary throughout the year and throughout the day.

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Water demand fluctuates according to the time of year, time of day, level of tourism, and other factors. Seasonal demands are typically the highest in the months of July and August, and the lowest in the months of January and February as shown in Figure 2. It is not uncommon for the District to experience a "hot spell" within the summer months resulting in many consecutive days of high water use. Sizing the system to accommodate these "hot spells" is essential in maintaining system reliability. For Nipomo, average annual water demand is approximately 1,065 gpm, including Black Lake. Average summertime demand is estimated to be 1,370 gpm. For purposes of assessing distribution system needs, the average summertime demands were simulated as the base demand condition.

Two demand conditions typically of interest when sizing components of water systems are the demand during the maximum usage day of the year (referred to as the maximum day demand) and the demand during the maximum usage hour of the day (referred to as the peak hour demand). The District's distribution system should also be capable of supplying the maximum day demand plus fire flow conditions at the minimum pressures stated in **Table 4**.

Purveyors typically do not keep daily or hourly water demand records. Nipomo is typical in this regard.

Based on system assessments in communities with similar populations, land use, and climate, maximum day demand is typically twice the average annual demand. Similarly, peak hourly demand has been found to be twice the maximum day demand.

These typical peaking factors were used to assess Nipomo's water system. For existing water demands, peaking factors are as follows:

Average Annual Demand	1,065 gpm (Main system)
Average Summertime Demand	1,370 gpm (Main system)
Maximum Day Demand	2.0 times Summertime Demand (2,740 gpm)
Peak Hourly Demand	4.0 times Summertime Demand (5,480 gpm)

Sewer

Regarding sewage flows, three flow conditions are of interest in sizing components of the wastewater collection system:

- 1. Average Dry Weather Flow ADWF refers to the average annual flow conditions in the system which generally occur during the summer at mid-day (i.e. not peak morning or evening flow conditions).
- Peak Dry Weather Flow PDWF refers to the peak anticipated daily flow which generally occurs in the morning or evening hours at which times residential flows reach their maximum. PDWF conditions do not include an inflow/infiltration component as would be expected during periods of rainfall.
- 3. Peak Wet Weather Flow PWWF is the maximum anticipated flow rate for a given system. PWWF refers to the peak anticipated daily flow which coincides with the occurrence of inflow and infiltration into the system. Inflow and infiltration is comprised of rainfall and runoff that enters the system through manholes, infiltration into gravity collectors resulting from high ground water, and illegal storm drain connections to the sanitary sewer system.

The District maintains records of monthly high flows as measured at the main treatment plant. For the 1993/95 period, the highest monthly flow recorded at the plant was 0.606 MGD, which is 1.93 times the average recorded monthly flow rate. This was compared to peaking factors referenced in other wastewater collection system assessments.

In general, small collection systems experience wider flow variations than large systems. For example, smaller tributary areas such as residential lift station tributary areas experience high flows in the mornings and early evenings. The collection system must be sized to handle peak flows, particularly peak flows that coincide with incidents of inflow and infiltration.

Sewage loading peaking factors for Nipomo are estimated to be:

Peak Dry Weather Flow	2.0 times ADWF (as compared to peak monthly flow of 1.93)
Peak Wet Weather Flow	3.0 times ADWF

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3.0 Existing Water System

3.1 Overview

A schematic of the District water system is shown on **Figure 5**. The water system is a single pressure zone system consisting of:

- Two storage sites (Twin Tanks and the Standpipe) each location with 1 million gallon capacity,
- 6 active wells, and
- A distribution system comprised of 6-, 8-, 10-, 12-, and 16-inch diameter pipes.

The Black Lake development is currently served by a separate water system consisting of:

- One 400,000 gallon storage tank accompanied by a 3,000 gallon hydropneumatic tank and pumping system,
- 2 active wells, and
- A distribution system comprised of 6- and 8-inch diameter pipes.

A significant feature of the existing water distribution system is the fact that the main zone and the Black Lake system currently are not intertied. Further, the central business district and the outlying residential rural areas of the District are separated by Highway 101 and Nipomo Creek. A single 10-inch diameter waterline along Tefft Street connects the two areas of the system.

Also, a new 16-inch diameter pipeline was recently constructed to allow water to be pumped from the Via Concha well to residential areas along Camino Caballo.

As is shown in **Figure 5**, the Twin Tanks are located at the easternmost portion of the District's water system near North Dana Foothill Road. The main downtown area of Nipomo is served by a 10-inch diameter pipe from the Twin Tanks in addition to the Church Well and the Savage Well, which is currently off-line.

The Standpipe is located off of Hetrick Avenue north of Cherokee Place. This area of the system is also supplied by the Bevington, Eureka, Olympic, Omiya, and Via Concha wells as shown in Figure 5. Regarding existing water system operations, it was noted that the Standpipe plays a key role in the hydraulic operations of the system. It fills first because it is closest to the District's largest wells and its water level can drop relatively rapidly at an average rate of emptying. Further, the Standpipe directly influences the available pressure in the Summit Station area. For example, if the Standpipe drops up to one-third, static pressures in Summit Station drop below 40 psi. Operationally, this means that operators try to keep the Standpipe full rather than allowing the tank level to fluctuate throughout the day to meet daytime demands.

3.2 Sources of Supply

Ground water is currently the sole source of water to the District. Historic production from each of the District's wells is tabulated in **Appendix A**.

There are currently six active wells used by the District for water delivery to the main system. The District has three wells that are on standby, and one that is not in operation due to water quality concerns. The Black Lake development area has two wells that support that system. **Table 6** lists data for existing wells.

PG&E tests performed in 1994 and 1995 indicate the flow rate, pumping water level, and motor efficiency for test conditions at each well. In general, pumps with efficiencies greater than approximately 65 percent are considered to be in "good" condition by PG&E. PG&E's pump tests indicate that all of the well pumps operate at efficiencies less than 65 percent.

Pumps with efficiencies in the 40 percent to 65 percent range are considered by PG&E to be in "fair to poor" condition. Pumps with efficiencies in this range included Black Lake #3, Bevington, Eureka, Olympic, and Omiya. Pumps with efficiencies of less than 40 percent were considered in "poor" condition. The Church Well pump fell into this category. PG&E test data was unavailable for the Black Lake #4 and Savage wells.

Upgrading the low efficiency pumps can result in a significant savings in power costs. For example, a PG&E test report indicated that Eureka Well had an efficiency of 62.5 percent. In addition, the test report stated that improving this efficiency by approximately 6.5 percent could result in an annual power saving of over \$8,200.

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Recommendations for well pump and motor replacements are included in Section 11.

Further, the Church and Savage Wells are located near Nipomo Creek but not so close that the provisions of the Surface Water Treatment Rule apply.

TABLE 6 EXISTING WELL DATA							
WELL	FLOW RANGE (1) (gpm)	MEDIAN FLOW (1) (gpm)	TYPICAL DEPTH TO GROUND WATER (feet)(1)	DATE DRILLED	PUMP MODEL	MOTOR TYPE	WELL STATUS
Bevington	392-410	401	317	6/85	Peerless Turbine	General Electric 100 HP	Active
Church	158	158	77	6/85	N/A	N/A 30 HP	Active
Eureka	780-820	800	148	6/79	Anderson Turbine	General Electric 200 HP	Active
Olympic	140-150	145	287	6/85	N/A	N/A 40 HP	Active
Omiya	120	120	312	6/88	N/A Submersible	N/A 30 HP	Active
Savage	125	125	74	6/88	N/A	N/A	Off-Line
Via Concha	703	703	286	N/A	Peerless Turbine	US Motors 150 HP	Active
Dana #1	N/A	N/A	N/A	N/A	N/A	N/A	Stand By
Dana #2	N/A	N/A	N/A	N/A	N/A	N/A	Stand By
Hermreck	N/A	N/A	N/A	N/A	N/A	N/A	Stand By
Black Lake #3	350	350	285	N/A	Peerless	N/A 50 HP	Active
Black Lake #4	400	400	N/A	N/A	N/A	N/A	N/A

N/A = Not Available

(1) Based on PG&E' pump tests performed 1990 and 1995

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3.3 Storage Facilities

Two storage facilities currently serve the District's water system: the Twin Tanks, and the Standpipe. These reservoirs provide daily regulatory, fire, and emergency storage.

The Twin Tanks consists of two 0.5 million gallon tanks, with diameters of 30 feet and heights of 24 feet. The reservoirs have a high water elevation of approximately 548 feet. A 10-inch diameter inlet/outlet line along Tefft Street connects the Twin Tanks to the distribution system.

The Standpipe is a 1.0 million gallon welded steel tank, with a diameter of 44 feet and a height of 90 feet. The reservoir has a high water elevation of approximately 548 feet. A 16-inch diameter inlet/outlet line along Hetrick Avenue connects the Standpipe to the distribution system.

3.4 Distribution and Transmission Pipelines

Plate 1 illustrates the existing water distribution and transmission system. The main distribution pipelines in the District are 8-inch diameter, with some 10-inch and 16-inch diameter pipelines. Pipelines extended from the east along Tefft Street, loop along Juniper Street, Division Street, Orchard and Pomeroy Roads. The 10-inch diameter pipeline extends to Hetrick Avenue which ties into the Standpipe. In addition, the 10-inch loops via Osage Road and Ridge Road back to Hetrick Avenue. The system also relies on an 8-inch diameter loop in the northern part of the system to provide water service to residences.

Overall, the water system is well- looped without numerous lengthy dead end pipes. One notable feature is that the main zone and the Black Lake system are not intertied. Also, the central business district and the outlying residential rural areas of the District are separated by Highway 101 and Nipomo Creek. A single 10-inch diameter waterline along Tefft Street connects the two areas of the system.

The material of existing pipelines within the District consist of asbestos cement, cast iron, ductile iron, polyvinyl chloride, and steel. The majority of the pipelines are asbestos cement and polyvinyl chloride.

4.0 Existing Sewer System

4.1 Overview

Approximately 40% of the water service area is connected to the Nipomo community sewer system. The sewage collection system consists primarily of a 10- to 12-inch diameter gravity line which extends along both sides of Highway 101 from Juniper Street south to the main wastewater treatment plant. **Figure 6** illustrates principal features of the sewage collection system.

The District operates seven sewer lift stations in addition to the lift station at the main treatment plant. Wastewater from two areas operated by the County of San Luis Obispo is also introduced into the District's sewer system.

As was previously mentioned, the Black Lake development is on a separate sewage collection and treatment system which is operated by the District.

4.2 Lift Stations

The District's sewer system includes eight lift stations that pump sewage to the main wastewater treatment plant. There is an additional lift station located at the treatment plant headworks plus two lift stations that are operated by the County of San Luis Obispo.

TABLE 7 EXISTING SEWAGE LIFT STATIONS ¹					
LIFT STATION	CAPACITY (gpm)	HEAD (ft)	FORCE MAIN DIA. (in.)	ESTIMATED ADWF/PWWF (gpm)	
Main Plant	630	21	6	45/135	
Tefft Street	315	65	6	83/250	
Black Lake Mobile Home Park	175	54	4	21/65	
Nipomo Palms	175	58	4	16/50	
North Oak Glen	175	29	4	5/15	
Bracken	110	70	4	2/6	
La Mirada	190	41	4	11/35	
Gardenia	110	55	4	2/6	
Woodgreen ² (Black Lake)	175	60	4	N/A	
Peoples Self Help Housing (CSA 1) ³	210	-	-	171/515	
Galaxy Park ³ (CSA 1)	310	115	6	37/110	

The lift stations and capacities are as listed in Table 7. The location of each lift station is shown in Figure 6.

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 Information provided by District staff.
 Part of separate Black Lake sewage system.
 Peoples Self Help Housing and Galaxy Park Pump Stations are operated by the County and pump to the District's sewage collection system.

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All lift stations are equipped with two pumps with each pump capable of pumping the full capacity of the lift station.

4.3 Collection System

The District's sewer system is comprised of approximately 55,000 feet of pipe, including 12-inch diameter gravity collectors. All of the sewer system is polyvinyl chloride sewer pipe and is reportedly in good condition.

The majority of the lift station tributary areas (**Figure 6**) are comprised of 6- and 8-inch diameter PVC gravity collectors. The main collection system is comprised of larger diameter PVC, which takes flow by gravity to the treatment plant in the southern part of the District service area.

Force mains within the system are 4-inch and 6-inch diameter.

The District's sewer system also has approximately 200 sewer access manholes. The sewer system is currently without an operating flow metering in place.

5.0 Computer Modeling

5.1 Model Development

Hydraulic network computer models of the District's water and sewer systems were developed as part of this master plan to aid in analyzing the systems' needs and capabilities. Node and pipe maps for each of the models were submitted to the District in June 1995. Computer diskettes containing model input files will be transmitted with the final report. Background information on each of the models follow.

Water Computer Model

The Boyle developed computer software, BoyleNET, was used to model the District's water system. BoyleNET uses the Hazen-Williams formula as the basis for calculating headloss. Input to the model primarily consists of pipes and "nodes". Pipes are described by the length, size, and Hazen-Williams 'C' factor (or friction coefficient). Nodes are described by elevation and demand. Other water system facilities such as tanks and wells were modeled. Pump curves were available for each well with the exception of the Olympic Well, which was modeled as a fixed supply into the network.

An AutoCAD base map of the District, including streets and lot boundaries, was provided by the District. This was used in laying out the pipeline network and in estimating the demand area for each water system node.

The input file for the District's existing water system is included in **Appendix B**.

The computer model is a tool by which the hydraulic performance of the system can be simulated under various conditions. The District's existing system model was used to assess system adequacy to meet existing and projected demands.

Sewer Computer Model

Similar to the water system, a computer model was also prepared for the sewer system. Using Boyle developed software, BoyleSWAN, the characteristics of the existing sewage collection system were simulated on the computer.

Sewage collectors were described in terms of diameter, length, and roughness coefficient (Mannings 'n' value). Manholes were described in terms of invert elevation.

Sewage loading was estimated for each manhole based on the number of residential units or land use acreage tributary to each reach. The sewage duty factors listed in **Table 2** formed the basis for estimated loading.

Each lift station tributary area was assessed separately. The main gravity collection system to the treatment plant was assessed with fixed flows input to simulate the operation of lift stations.

Appendix B contains input files for the existing sewage collection system.

5.2 Model Calibration

After the computer models were developed, a series of calibration runs were performed to determine how closely the computer models simulate actual field conditions.

For the water system, the District's operations staff conducted a series of fire hydrant tests during June 1995. Fifteen fire hydrants were tested at various locations throughout the system. For each test, the static pressure was measured with a pressure gauge at a water service or other hydrant close to the test hydrant. Then the test hydrant was fit with a pitot measuring device and opened to full flow. At full flow, the pitot measurement and the residual pressure (taken at the same location as the static pressure) were read simultaneously. District staff was also asked to record tank levels and well status at the time of each hydrant test.

The existing demands, as estimated in Section 2.0, were used to simulate demand conditions. The demands were adjusted based on the

time of day and weather during which the tests were taken. Static conditions were first modeled and compared to field measured pressures. The assumed demands were then adjusted to achieve reasonable agreement with the field measurements. Once agreement was achieved, the field measured fire flow was modeled. If the modelcomputed residual was within five pounds per square inch (psi) of the field measured pressure, then the model was considered in reasonable agreement with the field measurement. Overall agreement with the field measurement is an indication that the computer model is calibrated and is modeling the actual conditions of the system with a reasonable degree of accuracy.

The results of the fire hydrant tests and calibration runs are included in **Appendix C**. Agreement within 5 psi was achieved at the majority of the sites tested. There were several locations where computer simulated pressures varied from field measurements. In these cases, hydrant tests were re-run.

The results of the water calibration exercise confirmed that the computer model is simulating existing water system performance within a reasonable degree of accuracy. Estimates of roughness coefficients and pipe size and layouts simulated in the model are considered representative of the Nipomo system.

Regarding the sewer system computer model, no flow metering was authorized to compare actual rates of flow to estimates. Lift station run time estimates were compared to estimated tributary area flows to achieve a reasonable degree of accuracy for each lift station.

Sewer model "calibration" consisted of an interview with District operations staff to confirm areas of projected capacity problems to staff observation. Computer projections of capacity problems were confirmed by staff observations.

The District may consider temporary flow metering during the rainy season to confirm the peaking factors estimated herein.

6.0 Design Criteria

This section summarizes the criteria that was used as a basis for analyzing the water and sewer systems' adequacy to meet existing and projected demands.

6.1 Water System Design Criteria

Design criteria for the water system is:

Supply facilities should be sized to meet maximum day demand with the second largest well out of service.

Storage capacity is required to provide daily regulatory storage, fire storage, and emergency storage. The following criteria was used to estimate these volume requirements:

• **Regulatory storage** is the volume of storage recommended to meet peak daily demands in excess of what supply is capable of producing. Supply facilities are sized to supply the maximum day demand (MDD) as stated above. For Nipomo, recommended regulatory storage volume is "maximum daytime demand" (i.e. 1.5 x MDD) less the available rate of supply over a 14-hour demand period, as follows:

Regulatory Storage Volume = $(1.5 - 1.0) \times (MDD) \times 14$ hrs.

- Emergency storage is the volume of storage recommended to ensure ongoing supply in the event of a water supply emergency. Emergency planning guidelines suggest that water facilities should be capable of sustaining basic sanitary needs for 72-hours. Thus, emergency storage for Nipomo has been estimated as the volume of water needed to provide a minimum of 50 gpcd for 72 hours.
- Fire storage is the volume of storage recommended to meet fire flow requirements for the duration indicated by the fire protection agency. The fire flow requirements listed on **Table 5** form the basis for the fire storage requirements in the District water service area. The highest requirement governs the fire storage requirements in that particular zone.

To analyze the adequacy of the **distribution pipelines** the following criteria was used:

- During **average day demand**, a minimum pressure of 40 psi and flow velocities less than 5 feet per second (fps) should be maintained. Maximum desirable static pressure is 100 psi.
- During **peak hour demand** conditions, a minimum system pressure of 30 psi and flow velocities in pipelines of less than 10 feet per second should be maintained.
- During **fire flow** conditions, the system should be sized to accommodate a minimum residual pressure of 20 psi at the flowing hydrant, and flow velocities in pipelines of less than 10 feet per second, at maximum day demand conditions.

The resistance of flow in a pipeline is represented by the **Hazen Williams 'C' coefficient**. 'C' values characterize the friction losses associated with the interior pipe wall and are a function of pipeline material, condition, and age. For pipelines with identical diameters and lengths, the lower the 'C' value, the higher the headloss. 'C' values were estimated based on the following criteria:

- All existing pipes: C = 125
- All proposed pipes: C = 135

These estimates of friction coefficients were used in calibrating the water computer model and found to be reasonable estimates for Nipomo.

Other design criteria utilized in assessing the District's water system is:

- Provide fixed emergency power generators for critical wells, particularly if seeking credit for emergency storage volume.
- Minimum new distribution main diameter 8-inches; 6-inch minimum in cul-de-sac streets that do not serve a fire hydrant.
- Replace all 4-inch diameter waterlines with 6-inch diameter lines or larger. Replace all existing steel pipelines with PVC or other material.
- Establish a goal of limiting unaccounted for water to 15% of production.

6.2 Sewer System Design Criteria

Regarding flow velocities, 2 feet per second minimum velocity should be maintained under peak dry weather flow conditions; 10 feet per second maximum at peak wet weather flow conditions.

Permissible flow depth in terms of depth (d) relative to pipe diameter (D):

- d/D = 0.5 maximum at average dry weather flow
- d/D = 0.75 maximum at peak dry weather flow
- d/D = 0.9 maximum at peak wet weather flow

Pipeline **roughness coefficient** 'n' estimated to be 0.011 for existing collectors.

Limit proposed collector and **manhole depth** to reasonable construction limitations (approximately 15 feet deep). Consider installation of a lift station at greater depths.

Lift stations must have sufficient capacity to handle the peak wet weather flow condition. Small lift stations (100 gpm and less) to be equipped with two pumps. Larger lift stations to be equipped with three pumps. In all cases, lift stations should be capable of handling peak wet weather flow with one pump out of service. Force mains should be sized to maintain 3 to 7 feet per second flow velocity.

Wet well volumes should be sized to minimize pump start/stops while avoiding septic conditions associated with infrequent purging.

Other design criteria used in assessing the District's sewer system are:

- Provide fixed emergency power generators for lift stations, particularly if alarm system is lacking or if consequences of an overflow would be significant.
- Minimum new gravity collector diameter to be 8-inches.
- Eliminate the need for lift stations where practical.
- Provide telemetric controls among lift stations to a control center.

These criteria were applied to the assessment of the existing water and sewer systems and in making recommendations for future system upgrades.

7.0 Ability of Water System to Meet Existing Demands

7.1 Sources of Supply

The design criteria stated in Section 6.0 indicated that sources of supply should be sized to meet maximum day demands with the second largest well out of service. Sources of supply must keep up with maximum demand during a 24-hour period and should have some redundancy, thus the second largest well out of service criteria.

For Nipomo, current maximum day demand, including Black Lake, is estimated to be 2,740 gpm.

The active wells listed in **Table 6** have a total estimated capacity of 2,900 gpm, including Black Lake Wells #3 and #4. Thus, the District needs nearly all active wells to be operable to meet estimated maximum day demand.

The two largest wells are the Eureka Well (800 gpm) and the Via Concha Well (700 gpm). By the supply source criteria stated herein, the District should have an estimated 540 gpm additional well capacity to reliably meet the needs of existing customers.

Another item of note in examining the existing system performance is the fact that the pump curves and pumping water levels given for the District wells indicate that the majority of the well pumps are operating at low efficiencies. The Eureka, Omiya, and Church wells in particular may be operating at low efficiencies. The District is encouraged to re-evaluate proper pump and motor sizing for all of the active wells.

7.2 Storage Facilities

By the criteria stated in Section 6.0, recommended storage volume to meet existing needs, including the Black Lake development, is:

Storage Component	Criteria	Volume Recommended
Regulatory	(1.5 - 1.0) x MDD over 14 hours	1.15 MG
Emergency	50 gpcd for 3 days Population 9,005	1.35 MG
Fire	3,000 gpm for 3 hours	0.54 MG
TOTAL		3.04 MG

The District currently has a total of 2.0 MG of storage in place. Thus, an additional 1.04 MG of storage is recommended to reliably meet the needs of existing customers.

An option to providing additional above-grade storage is to, in a sense, utilize the ground water basin as emergency storage. To do so reliably, natural gas driven engines or fixed emergency power generators should be maintained at key wells to ensure their availability during a prolonged power outage. At least 940 gpm of well capacity would need to be powered in such a way for reliable emergency back-up.

Further, it was noted in our existing system assessment that the Standpipe plays a key role in the hydraulic operations of the system. It fills first because it is closest to the District's largest wells and its water level can drop relatively rapidly at an average rate of emptying. Further, the Standpipe directly influences the available pressure in the Summit Station area. For example, if the Standpipe drops up to onethird, static pressures in Summit Station drop below 40 psi. Operationally, this means that operators try to keep the Standpipe full rather than allowing the tank level to fluctuate throughout the day to meet daytime demands. This operational sequence at the Standpipe means that the District cannot make full use of the 1.0 MG volume without significantly dropping system pressures to 40 psi and below.

There is no suitable terrain in the vicinity of Summit Station upon which to construct an elevated storage tank of more conventional proportions (1.5 diameter to 1 height). The District could operate the Summit Station area as a separate hydraulic grade zone and provide a booster station with hydropneumatic tank to serve the residences. Approximately 50 residences lie at elevations that pose water pressure problems under the current configuration. The advantages of serving a portion of Summit Station by a separate booster station are that:

- Fluctuations in water pressure could be minimized,
- Overall pressure could be raised to a hydraulic grade of approximately 570 feet such that minimum static pressure would be raised to 50 psi,
- The existing Black Lake hydropneumatic tank could possibly be relocated to service Summit Station, and
- Fluctuations in the elevation of the Standpipe would not significantly influence water pressure at Summit Station.

Disadvantages of installing a separate booster station are:

- Capital and operations cost associated with the operations of a booster station,
- Unacceptable high pressures (100 + psi) in some areas of the boosted zone,
- Increased system complexity (i.e. operation of a two-zone water system), and
- Level fluctuations at the Standpipe would continue to affect other areas in the eastern service area.

Considering these advantages and disadvantages, it is our opinion that construction of a booster station is not warranted to serve the existing 50 properties. The District may wish to re-evaluate this position as additional properties develop in Summit Station.

7.3 Distribution System Assessment

The BoyleNET hydraulic network computer model was used to simulate the ability of the existing distribution system to meet existing needs.

Following the design criteria stated in Section 6.0, a series of modeling runs were made with results as follows:

- Average Day Demand Average daily demands were modeled with both tank facilities assumed to be three quarters full (540 feet hydraulic grade line) and the Eureka and Bevington wells operating. Average system pressures were approximately 95 psi, with the lowest pressure of 47 psi in the Summit Station area. Pressures exceeded 100 psi in the vicinity of the wells along Willow Road. No deficiencies were noted with regard to meeting average day demand.
- 2. Peak Hour Demand Peak hourly demands were simulated throughout the system with tanks set at three-fourths full (540 feet HGL) and the Eureka, Bevington, Omiya, Via Concha, and Church wells operating. Average system pressures dropped to approximately 65 psi, with the lowest pressure of 25 psi along Grande Avenue and north of Juniper Street in the vicinity of Trevino Drive. Flow velocities were favorable throughout the system.
- 3. Fire Flow Conditions A series of maximum day demand plus fire flows were conducted. Overall, the existing system is found to be well laid-out to meet residential fire flow requirements. The exception to this is some of the high elevation areas in Summit Staion. A flow of 1,000 gpm at 13 psi is projected at Poppy Lane. Twenty psi minimum is recommended.

Commercial, public facility, and multi-family zoning fire flows presented a different case. Meeting the 3,000 gpm recommended flow in some areas posed a problem. This rate of flow cannot be sustained at the commercial retail property at the intersection of Grande Avenue and Orchard Road. Similarly, improvements would be needed to meet firefighting needs at the school along Price Street and at the residential multi-family property along Grande Avenue.

In addition to the specific demand conditions stated above, overall system reliability was also assessed. Specifically, the central business district and the outlying residential rural areas of the District are separated by Highway 101 and Nipomo Creek. A single 10-inch diameter waterline along Tefft Street connects the two areas of the system. Additional highway/creek crossings are recommended to improve system reliability as well as to improve distribution.

The Black Lake system intertie is discussed in Section 9.

Recommended improvements to meet existing demands are illustrated on **Plate 1**. A listing of the recommended facilities as well as priorities are included in Section 12.0.

It has been noted that some development throughout the service area consists of structures that lie at a significantly higher elevation than the District's distribution system. For example, a home that rests 15 feet higher than the District's water main will have a static water pressure that is 6 to 7 pounds less than pressure in the main. This has resulted in some pressure complaints and concerns regarding fire fighting.

The District has no control or authority governing building pad elevations. It is therefore recommended that the District continue enforcing its policy of meeting water pressure and fire flow requirements at the main and that owners of structures that lie at higher elevations be alerted to the need to provide private water pumps.

8.0 Ability of Sewer System to Meet Existing Needs

8.1 Lift Stations

Table 7 lists features of the existing lift stations, including estimated average dry weather and peak wet weather flows. Each of the eight lift stations currently operated by the District appear adequate to meet existing sewage flows.

Some of the lift stations appear over-sized to meet existing needs. For example, the Bracken, North Oak Glen, Nipomo Palms, and Gardenia lift stations all appear to have capacities that are far in excess of estimated flows. Operationally, this means that:

- 1. The wet wells are not permitted to fill and the relatively large pumps run for short periods, or
- 2. The wet wells are permitted to fill and conditions become septic in the wet well between pump starts. Odor and quality problems result.

In either case, the District should re-evaluate wet well volumes, pump and motor sizes, and on/off levels in the stations listed above.

Section 6.0 listed criteria for lift station design as follows:

- Small stations (up to 100 gpm) should be equipped with two pumps.
- Larger stations should be equipped with three pumps.

In both cases, lift stations should be capable of handling peak wet weather flows with one pump out of service.

The system was also evaluated for the possibility of eliminating one or more existing lift stations. There is an opportunity to eliminate the Nipomo Palms lift station by constructing a gravity line to the southeast. This is discussed as a future system improvement in Section 10.

8.2 Collection System Assessment

The BoyleSWAN sewer model was used to assess the existing collector system capacity. Results of the computer simulations are:

Tributary Area	Results
La Mirada LS	No capacity problems noted
Bracken LS	No capacity problems noted
North Oak Glen LS	No capacity problems noted
Nipomo Palms LS	No capacity problems noted
Gardenia LS	No capacity problems noted
Black Lake Mobile Home Park LS	No capacity problems noted
Tefft Street LS	No capacity problems noted
Main Gravity Zone to the Treatment Plant	Division Street 8" inadequate; Frontage Road 12" from Division Street south inadequate

Overall, the existing collector system has adequate capacity to handle average and peak wastewater flows. The exception to this is an area along Division Street and the Fronage Road as noted above. Capacity problems in this area are proposed to be addressed by routing the CSA 1 lift stations flow through the Nipomo Palms lift station triburary area and constructing new gravity collectors to eliminate the need for the Nipomo Palms lift station. This is illustrated in **Plate 4**.

Regarding the Black Lake collection system, the system was assessed for the projected flows indicated in **Table 4** and found to have adequate collection capacity to handle projected flows. The Black Lake collection and treatment system has been sized for and is intended to serve the Black Lake development only.

9.0 Ability of Water System to Meet Future Demands

9.1 Sources of Supply

Future water demand for build-out within the service area boundary illustrated in **Figure 5 and Plate 2** is estimated to be 2,580 AFY, 50 percent higher than current annual demand. Future maximum day demand is estimated to be 4,140 gpm.

Nipomo's current active wells have an estimated combined capacity of 2,900 gpm, including Black Lake Wells #3 and #4. With the second largest well out of service, available supply is 2,200 gpm.

A new 540 gpm well is recommended to reliably meet the needs of existing consumers, including Black Lake residents. Supplies totaling an additional 1,400 gpm in addition to the recommended 540 gpm are recommended to reliably meet the future needs of the District.

9.2 Distribution and Transmission Pipelines

The water system improvements discussed in Section 8 address the majority of the future distribution system needs. One noteworthy additional system improvements to meet future demands is to construct a new 10-inch diameter transmission main along the Frontage Road from Sandydale Road northwest to Summit Station Road.

Plate 2 illustrates the system improvements recommended to meet future water demands. Recommended facilities to tie in the Black Lake system to the main system are also shown. Further, facilities shown are based on continuing to serve Summit Station off of the main pressure zone and do not reflect facilities needed to install a booster station.

District staff indicated that older, steel waterlines in the area northeast of Highway 101 are in need of replacement. **Plate 2** indicates approximately 4,300' of older, steel lines to be replaced in coming years.

9.3 Storage Facilities

By the criteria stated in Section 6.0, recommended storage volume to meet future water demands, including the Black Lake development, is:

Storage Component	Criteria	Volume Recommended
Regulatory	(1.5 - 1.0) x MDD over 14 hours	1.74 MG
Emergency	50 gpcd for 3 days Population 15,000	2.25 MG
Fire	3,000 gpm for 3 hours	0.54 MG
TOTAL		4.53 MG

The District currently has a total of 2.0 MG of storage in place. Thus, an additional 2.53 MG of storage is recommended to reliably meet the needs of existing and future customers. Additional above-grade storage is recommended to be installed adjacent to the existing Twin Tanks.

An option to providing additional above-grade storage is to, in a sense, utilize the ground water basin as emergency storage. To do so reliably, natural gas driven engines or fixed emergency power generators should be maintained at key wells to ensure their availability during a prolonged power outage. At least 1,550 gpm of well capacity would need to be powered in such a way for reliable emergency back-up.

10.0 Ability of Sewer System to Meet Future Needs

10.1 Lift Stations

As was described in Section 2.0, average daily sewage flow is projected to increase from 0.35 MGD in the main Nipomo system to 1.13 MGD at build-out. Estimated capacities and projected tributary flows to each lift station are listed in **Table 8**.

PROJE	TABLE 8 ECTED LIFT STATION	FLOWS
Lift Station	Current Estimated Capacity (gpm) ¹	Projected Flows - ADWF/PWWF (gpm) ²
La Mirada	190	11/33
Bracken	110	6/18
North Oakglen	175	30/90
Nipomo Palms	175	16/48
Gardenia	110	11/33
Black Lake Mobile Home Park	175	24 / 72
Tefft Street	315	170 / 510
Proposed Amado Street	N/A	35 / 100
Galaxy Park (CSA 1)	310	100 / 300
Peoples Self Help Housing (CSA 1)	210	17 / 50
Main Gravity Zone to the Treatment Plant	630	370 / 1,110 ³

1 Refer to Table 7

2 Refer to Table 4.

3 Gravity flow only. Excludes allowance for tributary lift station flows.

The tributary areas that correspond to the lift station flows listed above are illustrated on **Plate 3**.

One new lift station is proposed to serve the area shown in **Plate 4.** The proposed Amado Street Lift Station is proposed to serve the residential suburban and agricultural area (based on future conversion to residential zoning) east of Highway 101.

Regarding the Nipomo Palms Lift Station, it is possible to eliminate the lift station by constructing approximately 2,700 feet of 12-inch gravity collector southeast of the lift station to Story Street. The sewer system master plan illustrated in **Plate 4** includes the construction of the replacement gravity lines. Concurrent with the elimination of the Nipomo Palms lift station, the flow from the two CSA 1 lift stations is proposed to be routed through the Beverly Drive residential area. Routing lift station flows in this manner will relieve flows in the Division Street 8-inch collector and along the Frontage Road.

Regarding the Tefft Street Lift Station, District staff has observed that the existing wet well volume is inadequate, particularly to handle flows during power outages. Increased wet well volume or provisions for fixed, emergency power generation are recommended.

10.2 Collection System Capacity

The BoyleSWAN computer model was used to simulate projected wastewater flows throughout the existing collection system. Proposed lift stations and recommendations for capacity upgrades at the Tefft Street Lift Station were simulated.

Again, the only deficiencies noted in the existing collection system was in the gravity collectors that comprise the main zone. Partucularly the gravity collectors south of Division Street to the wastewater treatment plant were found to lack capacity for projected flows.

Improvements needed to meet projected community sewer needs are illustrated in **Plate 4**. Local collectors which will be needed as development occurs will follow future street patterns and therefore cannot be accurately illustrated in a master plan.

Further, a question arose regarding sewering the area between Story Street and Southland Street. There is a depression there which precludes sewering south toward Southland Street. It appears that the lower elevation areas will need to be served with a small lift station. Bear in mind that 1"=1,000' scale, 20 foot contour interval mapping was used as the basis for this master plan and that design-level facility plans are not presented herein. More detailed topographic mapping is needed to make specific sewering recommendations in this area. ÷

11.0 Recommended Improvements

11.1 Estimated Costs and Priorities

Sections 7.0 through 10.0 discussed improvements needed to meet existing and projected water and sewer needs. Recommended improvements are summarized herein and budgetary cost estimates are provided for recommended facilities.

Boyle recommends that the District embark on a capital improvement program as described herein. Recommended improvements are illustrated on **Plates 1, 2, and 4**.

Cost Estimates

Opinions of probable construction cost are included for recommended pipeline construction and other improvements. The actual costs of specific projects may vary depending on many factors such as site conditions, the extent of existing utilities, environmental impact mitigation, and market conditions that are both unknown and not within the control of the District or Boyle.

Pipeline construction costs include materials, excavation, installation, backfill, valves and fittings (water), manholes (sewer), pavement replacement, and traffic control. A 25 percent contingency for design engineering, and permitting is included in these estimates. Right-of-way acquisition costs are *not* included in the estimates.

Туре	Diameter (inches)	Unit Cost (\$/LF)
PVC Waterline - Class 150	8	54
	10	62
	12	67
Gravity Sewer Line	8	60
anonomi and a the second s	10	66
	12	72
	15	85
	18	115
	21	130
Sewer Force Main	4	50
	6	58

Pipeline costs, including contingencies, are based on the following unit costs:

The estimated cost to construct additional water storage is \$0.50 per gallon which includes site grading, foundation, tank fabrication, erection, perimeter road, and fence. Sites which require mass grading may more than double this cost. Also, site acquisition costs are not included.

For the proposed Amado Street sewer lift station, a capital cost of 50,000 is estimated for this station (approximate capacity = 100 gpm).

The unit costs stated above were utilized in **Tables 9 and 10** to estimate the capital cost of recommended system improvements.

Priorities for System Improvements

Improvements recommended to correct water system deficiencies, in particular, are fairly extensive. Over 5 miles of new distribution lines are recommended as well as replacement of inefficient well pumps and construction of additional storage. Priorities have been assigned as follows: **Priority 1:** Two additional Nipomo Creek crossings are recommended as first priority system upgrades because of the current lack of redundancy in the distribution system. A \$100,000 budget for well pump replacement is also recommended as a top priority, so that the District can benefit from energy savings.

Priority 2: Paralleling the existing Twin Tank inlet/outlet line is in the second group of priorities. Providing additional storage, augmenting well supply, and completing well pump replacement are also second priority projects.

Priority 3: The final group of projects includes various distribution system upgrades needed to strengthen fire fighting capabilities.

Tables 9 and 10 list recommended water and sewer system improvements to meet existing and projected needs. In all, an estimated \$3.8 million in water and sewer improvements are recommended to meet existing systems deficiencies.

Future water and sewer system improvements are estimated to cost an additional \$3.4 million.

Note that some system improvements will be installed by developers and that not all recommended improvements will need to be financed by the District.

11.2 Additional Recommendations

During the course of working with District staff to compile information for this Master Plan, it was noted that the water meters throughout the Black Lake development have a different unit rating than the rest of the Nipomo system. Black Lake water meters measure in units of gallons while the rest of the system is measured in hundreds of cubic feet.

This difference in meter type has several disadvantages:

· Necessitates additional accounting to bill customers in Black Lake

- Opens up possibility for error in both meter reading and tabulating water usage
- Adds a level of complexity to the water rate structure

We recommend that the Black Lake water meters be replaced with "standard" water meters and that the District consider installing an automatic meter reading system throughout that development. Estimated Unit Costs: 8-inch dia waterline 10-inch dia waterline 12-inch dia waterline

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\$54 per LF \$62 per LF \$67 per LF

Additional Storage \$0,50 per gallon ÷

MPROVEMENTS TO MEET	EXISTIN	G NEEDS:		IMPROVEMENTS TO MEET FU	JTURE NE	EDS:	
Improvement	Length	Diameter	Estimated Capital	Improvement	Length	Diameter	Estimated Capital
	(feet)	(inches)	Cost		(feet)	(inches)	Cost
Priority 1							
				Provide additional 1.53			e705.00
Highway 101 Crossing /				MG storage		•	\$765,00
Thompson & Sea 10"							
(Tefft St. Crossing Under							
Construction)	6,500	10	\$403,000				
				Black Lake system			
Creek/Highway Crossing	1000000			interties - (3) at \$25,000			
South of Knotts Street	3,850	10	\$239,000	each	-		\$75,00
Budget for Well Pump			\$100,000	Frontage Road main	5,150	10	\$319.30
Replacement Replace Steel Line on	5	•	\$100,000	Frontage Road - Juniper	5,150	10	0313,30
W. Dana Street	1,050	8	\$57,000	to Tefft	1,400	8	\$75,60
Replace Steel Line on E.		-		Connect to proposed			
Price Street	1,200	8	\$65,000	Frontage Rd 10"	1,000	8	\$54,00
Replace Steel Line at				Leaf Street - Thompson			
Bennett Street	1,400	8	\$76,000	to Cedarwood	1,750	8	\$94,50
Replace Steel Line in W.							
Price/Mallagh	630	8	\$34,000	Cedarwood Bennett Street to new	1,470	8	\$79,38
				10"	1,700	8	\$91,80
				Extend Honey Grove to	1,100	U	\$51,00
Subtotal Priority 1 =	14,630		\$974,000	Southland	1,100	8	\$59,40
•	TRUE BOOK AN		Chenneller 199	Twilight Lane	650	8	\$35,10
Priority 2				Inga Lane	1,700	8	\$91,80
				Camino Caballo	700	8	\$37,80
Install Parallel							
Inlet/Outlet Line to Twin Tanks	9,800	12	\$657,000	LUIL Change angula	1,000	10	\$62,000
Install Additional 1.0 MG	9,000	12	3037,000	Hill Street main	1,000	10	402,00V
Storage Tank			\$500,000		1,200	8	\$64,80
Budget for Well Pump							
Replacement			\$75,000				
Pursue Additional Well				100000000	100000		2211000620
Capacity		-	\$200,000	TOTALS =	18,820		\$1,905,50
			\$1,432,000	TO MEET FUTURE NEED	JS		
Subtotal Priority 2 =			\$1,432,000				
Priority 3							
Upgrade on Frontage							
Road	1,300	10	\$81,000				
Grande Avenue	1.010		exco 000				
Upgrade Frontage Rd. from	1,910	8	\$103,000				
Summit Station Rd	4,500	10	\$279,000	1			
Frontage Road Upgrade	1,100	1.072	\$59,000				
Black Hawk Way							
Upgrade s/ of Grande	150	8	\$8,000				
Standpipe Tank to	15-15-0-14	3 85.6					
Frontage Rd.	3,000		\$162,000				
Loop Along Pomeroy	5,300 890		\$329,000 \$55,000				
Upgrade Along Hill St Loop to Serve Nipomo	690	10	\$55,000				
Elementary School	700	8	\$38,000				
Bonita Homes to		-					
Orchard (Fir Place)	800		\$43,000				
Poppy Lane Upgrade	1,000	10	\$62,000				
Subtotal Priority 3 =	20,650		\$1,219,000				
out of all Filolity 5 -	20,030		\$1,210,000	-			

Improvement	Length	Diameter	Estimated	-		
	(feet)	(Inches)	Capital Cost			
mprovements to Meet Exist	ing Needs:			Estimated Unit Costs:		
Nipomo Palms Lift				8-inch gravity collector	\$60	per LF
Station Elimination	2,600	12	\$187,000	10-inch gravity collector	\$66	per LF
Tie CSA 1 Lift Stations	2,000	12	0101,000	To-mon gravity conocion	400	POL
over to Nipomo Palms	12		\$15,000	12-inch gravity collector	\$72	per LF
				15-inch gravity collector		per LF
Subtotal Existing Needs =	2,600		\$202,000	18-inch gravity collector	\$115	per LF
				21-inch gravity collector	\$130	per LF
mprovements to Meet Futur	e Needs:			4-inch dia force main		per LF
Gravity Line Upgrades:						
Oakgien Ave. Upgrade	1,320	15	\$112,000			
(Freeway Crossing)	880	15	\$75,000			
Frontage Road Upgrade	850	12	\$61,000			
-10	1,050	15	\$89,000			
	1,300	18	\$150,000			
	1,110		\$144,000			
Lift Stations:						
Proposed Amado Street						
Lift Station						
100 gpm Lift Station	(.)		\$50,000			
4-inch dia force main	700	4	\$35,000			
Tefft Street Lift Station						
Upgrade			\$100,000			
New Gravity Collectors:						
Orchard Road Collector	2,600	8	\$156,000			
Hill Street Collector	1,500	8	\$90,000			
Railroad Collector N/ of						
Tefft Street	1,900	8	\$114,000			
Frontage Road N/ of						
Juniper Street	2,800		\$168,000			
Story Street Tie over Pradera Place	2,800	8				
Septic System	1227	1.50	\$1,500			
Southland Street	3,500	- 8	\$1,500			
Camino Caballo	2,500		\$150,000			
Subtotal Future Needs =	24,810		\$1,495,500			

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APPENDIX A

Water Production Records 1988-1995

	Gross rvice Water Usage ions per Conn.		305 C(C,1 305 SHC 1			1,383 827			1,475 688			1,485 344		1,490 700			1,526 889				1,593 435		1,649 707			1,706 650		1,739 467	1,749 5/1		1,757 1,072			917 661,1 508.1		1,790 445		1,849 931		1,917 928	1,917 710,1		
	No. of Service									24									8%								**							201									
	NAW	()																		*								~						9									
	TOTAL	(acre-feet)	* 0	10	0.00		69 1	0 0			1,014	~ ~	5 60	~ 9	2		~			1,134			- (0)					2 1,217		-		-			1,187	~ ~							
	TOTAL	(jeð)	12,056,264	21,494,528	28,600,528	32,799,600	39.540.77	35,901.00	29,617,060	22.099.66	330,494,824	14,992,912		30,151,132		53,644,316	37,769,512	29,664,18	21,995,68	0/8/100/805			34,753,576	41,638,916	49,454,768 39,231,852	35,028,840	27,567,540	396,518,298 18,534,692	25,183,664	25,127,564	40,240,156	42,291,904	36,467,396	33,575,476	386,745,172	21,380,000 21,721,000	20,676,000	34,110,000	39,562,000	50,797,000	51,007,000	30 359 000	Contraction of the local division of the loc
	NO	(acre-feet	30	8	8 5	105	132	119	87	23	1,075	\$ 0	32	8 8	131	1/9	125	10	12	B02'1	381	2 56	E	12	124	106	8	1269	8 9	113	173	168	146	119	1,458	76	19	164	159	145	130	110	
	PRODUCTION	e) · (je0)	12,659,152	22,139,304	29,715,796	34,308,516	43,099,760	36.658.608	31,465,368	23,562,000	13,000,004	15,817,208	23,095,996	31,303,800	42,658,440	45,194,908	40,677,736	31,622,448	23,315,160	245,392,545	19,403,120	22,856,360	36,113,360	49,026,164	52, 193,944 40,253,620	34,413,984	26,038,628	25,176,184	27,941,540	36,978,128	56,527,856	54,854,580	47,530,912	36,642,428	475,098, 932	24,669,040 22,502,632	20,661,168	53,356,336	51,782,544	55,162,000 47,284,000	42,205,000	35,696,000	
	TAL																			2								•				•			•								
	SUBTOTAL																																										
	B'Lake #4																															0											
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	Sher																															0 359,768	00	313,412		00	• •	923,780	11,968	• •	•		0
	Church																															306,680			ŝ	• •	55,352	313,412	311,916	727,000	525,000	83,000	819.000
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F95	ş																																	424,864						3,258,000			
NIPOMO CSD WATER AND SEWER MASTER PLAN VT-NO4-100-01, WATERUSE XLS, CMF 4-28-95	WATER PRODUCTION RECORDS (SALLONS) Earlington Om																																	4,710,904		15,330,260		11,106,304			4,089,000		
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236,356,772 115,972,912 22,476,652 20,946,978 24,839,088 0 506,640 2,044,000 14,186,558 0 1,662,520 2,661,000 14,156,558 0 1,662,500 566,000 14,550,588 6,283,200 356,000 356,000 21,530,844 6,283,200 352,000 356,000 21,530,544 4,377,0102 2,998,000 3,932,000 21,530,544 1,6473,204 5,039,000 3,932,000 21,105,54 16,473,204 5,038,000 2,958,000 21,105,544 16,473,204 5,036,000 2,936,000 31,590,376 16,33,317 3,696,000 2,359,000 31,591,102,544 16,347,3204 5,561,000 2,936,000 31,710,122 1,253,316 5,550,000 3,654,000 0,657,000 31,471,132 1,457,750 3,554,000 3,654,000 0,675,000		3,615,096 1,519,256 1,519,212 1,515,212 6679,322 679,325 580,448 580,448		•	20, 625, 000 68,000 1,454,000 213,000			46,679,094 33,643,456	2	26,300,000	81		2,516	394
24,838,088 0 508,640 2 14,186,568 0 1,652,570 2 14,233,682 11,651,312 1,600,000 27,530,686 6,513,200 842,000 31,530,444 13,740,012 2,098,000 2 31,50,444 13,740,012 2,098,000 2 37,140,578 16,931,812 3,098,000 2 37,140,578 16,931,812 3,098,000 2 37,140,578 16,931,812 3,098,000 2 37,441,892 12,633,915 6,6581,000 2 34,541,892 14,553,916 6,535,000 2 34,541,892 14,553,916 6,535,000 2		1,319,256 1,156,212 666,5212 679,522 3,225,376 1,413,720 448 660,448 1,284,316			66,000 0 1,454,000 213,000	4,885,000 2,700,000 4,178,000 8,697,000 6,861,000	4,933,000 2,700,000 5,632,000 6,910,000 7,507,000 9,375,000	33,643,456	1,678 3	378,400,000	1, 161	31%		
0 508,640 2 0 1,882,530 2 11,851,312 1,503,000 6,283,500 882,000 1,375,212 3,439,000 1 1,770,012 2,088,000 2 16,473,204 5,591,000 2 16,893,812 3,696,000 2 14,575,3916 3,559,000 1 1,455,5316 3,550,000 1 1,455,5316 3,550,000 1 1,455,5316 3,550,000 1 1,455,5316 3,550,000 1 1,455,5316 3,550,000 1 1,455,550,000 1 1,455	nana na na	1,319,256 1,136,212 866,332 679,332 3,225,376 1,113,720 580,446 1,284,316			66,000 0 1,454,000 213,000	4,865,000 2,700,000 4,178,000 8,697,000 6,861,000	4,933,000 2,700,000 5,632,000 6,910,000 7,507,000 9,375,000	33,643,456						
0 1,852,320 2 11,851,312 1,563,000 6,233,200 832,000 4,876,212 3,439,000 1 1,6,473,204 5,591,000 2 15,653,912 3,656,000 2 1,4573,2915 3,569,000 2 1,4573,2915 3,559,000 2 1,4573,2915 3,599,000 2 1,4573,2915 3,599,000 2 1,4573,2915 3,599,000 2 1,4573,2915 3,599,000 2 1,4573,295 3,599,0	i da de ese	1,136,212 866,932 679,532 3,225,376 580,448 580,448			0 1.454,000 213,000	2,700,000 4,178,000 8,697,000 6,861,000	2,700,000 5,632,000 6,910,000 7,507,000 9,375,000		103	22,800,000	20		2,514	432
11.851.312 15.000 00 1.851.312 15.000 1 4.875.372 3.439.000 1 13.740.012 2.098.000 2 15.930.012 3.068.000 2 15.933.016 3.559.100 1 1.457.501 5.551.000 1 1.457.501 5.551.000 1	3 * 3 . 200 - 200	866,932 679,932 3,225,376 580,448 580,448			1,454,000 213,000	4,178,000 8,697,000 6,861,000	5,632,000 6,910,000 7,507,000 9,375,000	22,846,300	20	26,900,000	63		2,514	325
6.283,200 882,000 1 1,376,212 3,419,000 1 1,3,74,0,012 2,098,000 2 16,473,304 5,591,000 2 16,993,612 3,696,000 2 1,453,5916 2,554,000 1 1,453,5916 2,554,000 1	AK 12 - 20	679,932 3.225,376 1,413,720 580,448 1,284,316			213,000	6,697,000	6,910,000 7,507,000 9,375,000	34,757,936	107	20,400,000	63		2,514	4
4,876,212 3,439,000 1 13,740,012 2,099,000 2 16,473,204 5,509,000 2 16,993,815 3,55,000 1 12,533,816 5,55,000 1 14,573,816 5,55,000 1		3.225,376 1,413,720 580,448 1,284,316				6.861.000	7,507,000	42,661,020	131	30,600,000	16		2.514	3
13,740,012 2,098,000 16,473,204 5,691,000 16,993,012 3,696,000 12,653,916 6,53,000 14,627,758 2,654,000	dia 100	1,413,720 580,448 1,284,316			646,000	- 117 000	9,375,000	49.066.988	151	30,500,000	16		2.514	3
16,473,204 5,691,000 16,993,812 3,696,000 12,653,816 635,000 3,457,778 2,640,000	252	580,448	• •		1,963,000	1,412,000		63,978,380	196	56,600,000	174		2.514	84
16,993,812 3,696,000 12,653,916 635,000 3,452,768 2,554,000	***	1,284,316	0	0 60.770,176	2,683,000	ੰ	10,404,000	71.174.176	218	46,300,000	142		2.514	16
12,653,916 635,000				0 59,123,104	2,521,000	с 	10,279,000	69,402,104	213	69,500,000	213		2,514	60
3 452 768 2 594 000		0	0	0 48,893,806	2,035,000	7,079,000	9,114,000	58,007,806	178	46,300,000	142		2,514	76
NY 100'T 001'701'0		217,668	0 248,336	6 40,146,044	460,000	6,957,000	7,417,000	47,563,044	146	37,400,000	115		2,514	19
1,712,172 485,000		•	0 154,836	25	265,000	4,686,000	4,951,000	33,713,548	103	34,800,000	107		2,514	Ŧ
17,339,388 1,666,000		728,552		0 27,926,832	5,000	4,875,000	4,860,000	32,806,832	101	29,900,000	92		2,514	42
306,614,176 105,375,996 25,165,160 23,676,000	10,472 11	11,452,412	0 3,225,376	6 475,519,592	12,313,000	71,789,000 8	84,102,000 5	559.621,592	1.718 4	152,000,000	1,387	3651		
1,735,360 684,000		1,217,744	0 1,309,000		0	2,065,000	2.085,000	22,248,736	89					
	0	0	0 32,164	4 22,553,000	•	3,340,000	3,340,000	25,893,000	79					
9,975,328 11,402,512 1,273,000 1,791,000	0	0	0 10.472	24,452,312	507,000	2,698,000	3,205,000	27,657,312	85					
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							-	450,047,104		394,372,024		12%		673
O. VEAP AVEPAGES								MGIVear	AFY .	MG/year	AFY	MAW	ä	Dallconn/day
AVENAGES								CPC'DCL'CO		000'007'01		No.		
Jan 88 thru Jun 91 - Data sheets provided by Niporno CSD tilled "SLO Courty Engineering Dept. Water Jul 91 thru Mar 95 - Production records provided on Niporno CSD data forms. Contrangion data taken from None of Water Resonces Dydde Water Scatam Satiefics" form	Courty Engine forms. Consur n Statietics" to	oting Dept. Water Us mplion data taken sm	Usage."											
No. of service connections taken from above references. Water usage per connection based on production records.	per connection	based on production	n records.											

WATERUSE XLS

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SLO OFFICE

Page 2

\$5/00/8

APPENDIX **B**

Input Files for Water and Sewer Models

* EXIS * RECO * THIS NEW OUTPUT TITLE	MMENDED IS THE c:\engr c:\engr WATER M/ ODEL 0 S 2.0 50 80	OMO CSD TO CORRE FINAL FI \net\nip \net\nip ASTER PL 0 0 0	WATER DI CT EXIST LE FOR T .wrk loop.out AN VT-NO	ISTRIBU TING DE THE EXIS L D4-100-0	FICIENCIE STING SYS D1 CMF/JA 0.0 15	S INCLUD TEM L 8/26/9 .0 2 * TWIN T. * STANDP	5 0.0 125. ANKS	0 1918.			
	181 185 169 244 VALVES R PUMPS	-10.2 23 -65 222	2 3 5 4			* OMIYA (* VIA CO	TON WELL WELL PUMP NCHA WELL WELL PUM	PUMP			
PRV PUMP CI											
1	0	990	400	910	650	840	850	740	1020	680	* EUREKA
ż	ŏ	875	200	875	300	830	416	677	450	600	* BEVINGTON
3	0	952	40	924	80	826	100	749	120	630	* OMIYA
4	0	774	100	608	200	440	225	391	250	340	* CHURCH
5	0	936	200	888	400	856	700	696	800	576	* VIA CONCHA
PIPES 101	101	103	E(10	10	105						
102	101 102	102 103	5610 1560	10 10	125 125						
103	103	104	510	10	125						
104	104	105	520	10	125						
105	105	106	350	10	125						
106	106	107	430	10	125						
107	107	108	500	10	125						
108	108	109	830	10	125						
109	109	110	860	10	125						
110 111	110	111	1080	10	125						
112	111 112	112 113	1030 830	10 10	125 125						
113	113	114	320	10	125						
114	114	115	200	10	125						
115	115	116	60	10	125						
116	116	117	250	10	125						
117	117	120	360	10	125						
118	120	121	30	10	125						
119	121	122	260	10	125						
120	122	123	340	10	125						
121 122	123 124	124 125	25 440	10 10	125 125						
123	125	125	10	10	125						
124	126	127	320	10	125						
125	127	130	190	10	125						
126	130	131	30	10	125						
127	131	701	330	10	125						
128	118	700	200	10	125						
129	701	132	120	10	125						
130 131	118 134	134 135	700 1150	10	125						
132	135	136	870	10 10	125 125						
133	136	702	420	10	125						
134	137	138	800	10	125						
135	138	139	710	10	125						
136	139	140	710	10	125						
137	109	141	1340	10	125						
138	141	142	490	10	125						
139	142	143	620	10	125						
140	143	144	530	10	125						
141	144	145	270	10	125						
142	145	146	510	10	125						
143 144	146 147	147 150	340 250	10 10	125 125						
145	150	151	470	10	125						
146	151	140	440	10	125						
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147 148 150 151 152 153 154 155 157 158 160 161 162 163 166 167 168 90 171 172 174 177 176 177 177 178 90	140 152 153 155 156 157 160 162 163 166 167 171 172 174 176 180 185 184 180 185 183	152 153 154 155 168 157 158 159 160 161 162 163 164 165 166 167 170 171 172 173 169 175 176 177 176 175 179 180 179 182 184 182 187	760 700 540 160 700 650 630 25 650 40 510 80 370 240 150 510 370 240 150 510 370 2160 3650 1800 1700 900 900 198 5974 10 1130 357 250 10 1260	10 10 10 10 10 10 10 10 10 10 10 10 10 1	125 125 125 125 125 125 125 125 125 125		225 226 227 228 229 230 231 232 233 234 235 236 237 238 239 240 241 242 243 244 245 244 245 244 245 244 245 244 245 251 252 253 254 255 256 257 258	229 230 231 232 232 233 233 234 235 255 257 240 255 257 240 255 241 242 244 243 242 244 243 242 246 247 246 249 219 250 248 251 255 255 240 248 249 219 250 248 251 255 255 240 255 240 255 240 241 242 242 245 245 240 255 255 255 240 255 240 255 255 255 240 255 240 241 242 242 245 255 255 255 240 240 240 240 240 240 240 255 255 255 240 240 240 240 240 240 240 240 240 240	240 231 232 233 247 234 235 255 256 257 258 257 258 257 258 257 258 257 243 245 247 248 249 254 251 252 254 259 254 259 254	370 430 270 430 270 450 290 70 520 550 70 200 600 150 520 370 370 420 150 89 750 380 880 280 520 650 520 520 350 430 490 520 350 430 490 150 200 550 70 550 70 550 70 200 550 70 550 70 550 70 550 550 70 550 55	666666666666888668888888888888888888888	125 125 125 125 125 125 125 125 125 125
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303	294	295	510	6	125		381	360	362	260	6	125
304	295	296	530	6	125		382	362	363	400	6	125
305	296	297	860	6	125		383	362	364	660	6	125
306	297	298	1000	6	125		384	357	356	260	6	125
307					125		304		330		0	
	298	299	200	6	125		385	356	361	280	6	125
308	299	300	300	8	125		386	361	363	260	6	125 -
309	300	301	540	8	125		387	363	364	260	6	125
310	301	118	480	8	125		388	150	357	150	6	125
311	299	302	770	6	125		389	145	364	150	6	125
312	302	303	560	6	125		390	353	369	680	6	125
313			400		125			333	309	000	0	125
313	303	304		6	125		391	144	365	140	6	125
314	303	269	450	6	125		392	365	367	640	6	125
315	269	304	830	6	125		393	365	366	260	6	125
316	304	305	380	6	125		394	366	367	370	6	125
317	305	306	780	6	125		395	366	368	260	6	125
318	112	307	200	8	125		396	367	703	450	6	125
319	307	308	500	8	125		397	143	368	140	ž	125
								145	300		6	125
320	306	310	520	6	125		398	153	370	1800	6	125
321	310	309	300	6	125		399	369	370	380	6	125
322	309	116	570	6	125		400	221	371	570	8	125
323	121	311	520	6	125		401	371	372	1000	8	125
324	311	312	670	6	125		402	372	373	1620	8 8	125
325	312	122	200	6	125		403	373	374	280	8	125
326	123	313	300	6	125			77/	775	200	0	125
320	717				125		404	374	375	310	8	125
327	313	314	630	6	125		405	375	376	650	8	125
328	126	314	540	6	125		406	374	377	650	8 8	125
329	127	315	590	6	125		407	376	377	230	8 6	125
330	131	315	340	6	125		408	376	339	800	6	125
331	315	316	160	6	125		409	339	141	1240	6	125
332	316	317	675		125			155		1240	2	125
332				6	125		410	155	380	850	6	125
333	316	320	760	6	125		411	220	380	390	6	125
334	317	320	180	6	125		412	380	381	940	6	125
335	320	133	398	6	125		413	381	157	760	6	125
336	320	301	500	6	125		414	381	203	750	6	125
337	135	321	560	6	125		415	381	382	640	6	125
338	321	322	160		125		415	201	102		0	125
330	321	302		6	125		416	382	158	770	6	125
339	322	323	150	6	125		417	382	383	370	6	125
340	323	324	260	8	125		418	383	204	380	6	125
341	324	326	430	8	125		419	383	206	780	6	125
342	323	325	440	8	125		420	163	384	450	6	125
343	325	326	260	8	125		421	384	385	320	6	125
344	325	327	210	8	125		422	385	386			
345	327						422			600	6	125
	521	132	930	8	125		423	386	208	170	6	125
346	327	130	980	8	125		424	165	378	590	6	125
347	322	328	470	6	125		425	378	387	210	8	125
348	328	329	360	6	125		426	387	388	600	8	125
349	329	330	360	6	125		427	388	210	350	8	125
350	330	331	1020	8	125		428	170	389	180	8 8	125
351	331	332	360	8	125		429	389	390			
										430	8	125
352	332	333	210	8	125		430	390	391	590	8	125
353	332	318	800	6	125		431	391	212	310	8	125
354	318	116	550	6	125		432	160	392	720	6	125
355	333	319	200	6	125		433	163	393	780	8	125
356	319	114	900	6	125		434	165	394	620	8	125
357	138	342	660	8	125		435	394	395	550	8	125
358	342	343	330	8	125						°	
359	343						436	209	397	1210	6	125
		344	1220	8	125		437	397	400	600	8	125
360	344	345	820	8	125		438	400	207	980	6	125
361	345	346	890	8	125		439	400	401	910	8	125
362	346	347	900	6	125		440	401	205	980	6	125
363	346	338	420	8	125		441	401	201	510	10	125
364	338	347	600	8	125		442	397	402	420	10	125
365	347	330	1970	8	125		443	402	217	470		
					125						8	125
366	152	348	520	6	125		444	402	200	1660	10	125
367	348	349	170	6	125		445	190	403	2530	8	125
368	349	350	270	6	125		446	403	404	1230	8	125
369	349	351	600	6	125		447	404	407	2150	8	125
370	350	351	410	6	125		448	404	405	1020	8	125
371	351	352	560	6	125		449	405	406	390	8	125
372		352			125					1270		125
372	350		220	6	123		450	406	407	1270	8	125
373	352	151	130	6	125		451	406	408	1100	8	125
374	348	353	860	6	125		452	405	410	3700	8	125
375	353	354	200	6	125		453	408	704	500	8	125
376	354	357	950	6	125		454	192	411	1630	8	125
377	354	355	150	6	125		455	411	410	80	8	125
378	355	356	600	6	125		456	410	409	1600	8	125
379	355	360	260	6	125		450					
380				6	125		457	411	412	950	8	125
300	360	361	400	0	125		458	412	413	350	8	125

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459	412	430	1030	8	125	
460 461	414 191	193 421	1730 1120	8 8	125 125	
462 463	403 407	422 423	560 670	8 8	125 125	
464	408	424	1000	8	125	
465 466	414 147	425 420	480 590	8 6	125 125	
467	420	419	380	6	125	
468 469	419 146	139 416	570 640	6	125 125	
470	416	417	40	6	125	
471 472	417 418	418 419	330 300	6	125 125	
473	417	415	220	6	125	
474 475	415 418	343 342	470 690	6 8	125 125	
476	125	334	180	6	125	
477 478	334 334	335 336	440 250	6	125 125	
479	336	337	700	6	125	
480 481	124 335	335 427	150 290	6	125 125	
482	427	337	230	6	125	
483 484	337 427	426 428	440 440	6	125 125	
485	426	428	220	6	125	
486 487	428 426	122 340	400 240	6	125 125	
488 489	340 340	120 341	570 580	6	125	
490	340	117	290	6	125 125	
491 492	399 398	398 385	348 200	8 8	125 125	
493	169	174	332.6	8	125	
500 501	700 133	133 132	230 400	10 10	125 125	
502	702	137	200	10	125	
503 504	703 704	368 409	190 2760	6 8	125 125	
505	168	156	700	10	125	
506 507	156 194	168 198	750 2084	6 12	125 125	
508	198	199	2049	16	125	
509 510	159 104	392 226	1642 410	6 8	125 125	
511	103	227	410	6	125	
512 513	106 409	224 430	410 1100	6 8	125 125	* DALE AVE
514	430	710	2570	8	125	* FRISCO WAY
575 NODES	710	414	1890	8	125	* SUMMIT STATION RD
101 102	0	523.8 360	0	0	0	
102	0	342	0	0	0	
104 105	0 0	336 329	0	0	0	
106	0	324	0	0	0	
107 108	0	316 320	0	0 0	0	
109	0	328	0	0	0	
110 111	0	334 331	0	0	0	
112	0	310	0	0	0	
113 114	0	333 343	0	0	0	
115	0	350	0	0	0	
116 117	0	351 357	0	0	0	
118	0	329	0	0	0	
120 121	0	356 355	0	0 0	0	
122 123	0	343 337	0	0	0	
124	0	337	0	0	0	
125 126	0	333 333	0	0	0	
127	õ	327	ō	õ	õ	
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130 131	0	326 326	0 0	0	0	
132	0	343	0	0	0	
133 134	0 0	338 349	0	0	0	
135	0	368	0	0	0	
136	0	389	0	0	0	
137 138	0 0	395 362	0	0	0	
139	0	358	0	0	0	
140 141	0 0	365 346	0	0	0	
142	Ö	348	0	õ	0	
143	0	370	0	0	0	
144 145	0	367 372	0	0	0	
146	õ	373	õ	ŏ	õ	
147	0	356	0	0	0	
150 151	0	353 360	0	0	0	
152	0	374	0	0	0	
153	0	347	0	0	0	
154 155	0	365 361	0	0	0	
156	0	343	0	0	0	
157	0	322	0	0	0	
158 159	0	330 330	0	0	0	
160	0	340	0	0	0	
161 162	0	340 340	0	0	0	
163	ŏ	340	õ	0	ō	
164	0	340	0	0	0	
165 166	0	335 330	0	0	0	
167	ŏ	315	õ	ŏ	ŏ	
168	0	340	0	0	0	
169 170	0	-65.6 306.4	0	0	0	* VIA CONCHA WELL
171	ŏ	305	õ	õ	õ	
172	0	225	0	0	0	
173 174	0	254 267	0	0	0	* VIA CONCHA WELL DISCHARGE
175	ŏ	283	õ	ō	ŏ	VIA CONCHA WELL DISCHARGE
176	0	283	0	0	0	
177 178	0	183 - 15	0	0	0	* EUREKA WELL DISCHARGE * EUREKA WELL
179	õ	322	õ	õ	õ	
180	0	325	0	0	0	* BEVINGTON WELL DISCHARGE
181 182	0	-10.2 394	0 0	0	0	* BEVINGTON WELL
183	0	394	õ	0	0	
184	0	380	0	0	0	* OMIYA WELL DISCHARGE
185 186	0	23 362	0	0	0	* OMIYA WELL
187	0	362	0	0	0	
190 191	0	410 410	0	0	0	
192	ō	430	õ	0	õ	
193	0	428	0	0	0	
194 195	0	404 410	0	0	0	
196	0	380	õ	0	0	
197	0	367	0	0	0	
198 199	0	400 459.63	0	0	0	* STANDPIPE TANK
200	0	370	0	0	0	
201 202	0	357 357	0	0	0	
202	õ	343	0	0	0	
204	0	340	0	0	0	
205 206	0	347 347	0 0	0	0	
208	ö	347	0	0	0	
208	0	345	0	0	0	
209 210	0 0	330 328	0	0	0	
211	o	328	0	0	0	

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212	0	325	0	0	0		294	0	318	•	0	0
212								0		0	0	0
213	0	336	0	0	0		295	0	320	0	0	0
214	0	361	0	0	0		296	0	320	0	0	0
215	0	370	0	0	0		297	õ	320	õ	ŏ	ŏ
216	0	359	0	0	0		298	0	319	0	0	0
217	0	359	0	0	0		299	0	319	0	0	0
218	0	313	0	0	0					_		
210							300	0	318	0	0	0
219	0	350	0	0	0		301	0	319	0	0	0
220	0	360	0	0	0		302	0	310	0	0	0
221												
221	0	368	0	0	0		303	0	302	0	0	0
222	0	317	0	0	0		304	0	305	0	0	0
223	0	317	0	0	ō		305	ō	304	õ		ō
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224	0	317	0	0	0		306	0	306	0	0	0
225	0	319	0	0	0		307	0	318	0	0	0
											13776	
226	0	325	0	0	0		308	0	322	0	0	0
227	0	331	0	0	0		309	0	314	0	0	0
228	0	337	0	0	0							
LLO							310	0	309	0	0	0
229	0	347	0	0	0		311	0	328	0	0	0
230	0	307	0	0	0		312	0	335	0	0	0
231												
	0	311	0	0	0		313	0	324	0	0	0
232	0	315	0	0	0		314	0	306	0	0	0
233	0	321	0	0	Ō			ŏ	312	õ		ŏ
27/							315				0	
234	0	321	0	0	0		316	0	312	0	0	0
235	0	327	0	0	0		317	0	314	0	0	0
236	0	337										
230			0	0	0		318	0	359	0	0	0
237	0	338	0	0	0		319	0	348	0	0	0
240	0	361	0	0	0			0	310	0	1976	
240							320				0	0
241	0	308	0	0	0		321	0	397	0	0	0
242	0	313	0	0	0		322	0	398	0	0	0
243		311										
	0		0	0	0	* CHURCH WELL DISCHARGE	323	0	404	0	0	0
244	0	222	0	0	0	* CHURCH WELL	324	0	397	0	0	0
245	0	316	0	0	0			õ	398	õ	õ	õ
							325				1.17	0
246	0	318	0	0	0		326	0	399	0	0	0
247	0	318	0	0	0		327	0	362	0	0	0
248	0	315	0							1756		
				0	0		328	0	397	0	0	0
249	0	320	0	0	0		329	0	358	0	0	D
250	0	379	0	0	0				354			
251	ě						330	0		0	0	0
251	0	316	0	0	0		331	0	344	0	0	0
252	0	323	0	0	0		332	0	340	0	0	0
253	0	335	0	Ō	õ							
							333	0	337	0	0	0
254	0	370	0	0	0		334	0	337	0	0	0
255	0	361	0	0	0		335	0	340	0	0	0
256												
200	0	338	0	0	0		336	0	347	0	0	0
257	0	361	0	0	0		337	0	350	0	0	0
258	0	377	0	Ō							(17)	
250					0		338	0	342	0	0	0
259	0	336	0	0	0		339	0	360	0	0	0
260	0	331	0	0	0		340	0	374	0	0	
261	ō	329										0
			0	0	0		341	0	364	0	0	0
262	0	328	0	0	0		342	0	326	0	0	0
263	0	324	0	0	0			0.000				
					2053		343	0	320	0	0	0
264	0	321	0	0	0		344	0	350	0	0	0
265	0	353	0	0	0		345	0	360	0	0	0
266	0	362	0									U
200				0	0	¥.	346	0	360	0	0	0
267	0	345	0	0	0		347	0	353	0	0	0
268	0	313	0	0	0		348	0	372	0	0	0
269												0
	0	285	0	0	0		349	0	371	0	0	0
270	-	334	0	0	0				362	0	0	0
271	0						350	0	207		-	õ
			0		0		350	0			0	
272	0	328	0	0	0		351	0	342	0	0	0
272	0	328 320	0	0	0		351 352	0	342 361	0	0	0
273	0	328		0			351 352	0	342 361	0	0	0
273	000	328 320 336	0	0 0 0	0		351 352 353	000	342 361 361	0 0 0	0	0
273 274	0 0 0	328 320 336 330	0 0	0 0 0	0 0 0		351 352 353 354	0000	342 361 361 370	0 0 0	0 0 0	000
273 274 275	0 0 0 0	328 320 336	0000	0 0 0 0	0		351 352 353	000	342 361 361	0 0 0	0	000
273 274 275	0 0 0 0	328 320 336 330 323	0000	0 0 0 0	0 0 0		351 352 353 354 355	00000	342 361 361 370 387	00000	0 0 0	0000
273 274 275 276	0 0 0 0	328 320 336 330 323 338	00000	0 0 0 0	000000		351 352 353 354 355 356	000000	342 361 361 370 387 360	000000000000000000000000000000000000000	0 0 0 0	000000
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1999 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 -	242	0.000		1.01.214				
374	0	360	0	0	0		120	-1.58
375	0	360	0	0	0		121	-1.81
376	0	360	0	0	0		122	-2.48
377	0	360	0	0	0		123	-1.81
378	0	380	0	0	0		124	-1.58
380	0	380	0	0	0		125	-36.68
381	0	360	0	0	0		126	-1.81
382	0	369	0	0	0		127	-2.26
383	0	360	0	0	0		130	-3.38
384	0	340	Ō	0	õ		131	-1.35
385	0	359	Ō	0	0		132	-1.5
386	ō	320	õ	õ	õ		133	-5.36
387	0	342	ō	0	Ō		134	-3.91
388	Ō	317	ŏ	ŏ	ŏ		136	-2.63
389	ō	317	ō	õ	ō		137	-0.75
390	ŏ	339	ŏ	õ	ŏ		138	-1.5
391	õ	316	ŏ	õ	õ		139	-26.14
392	õ	317	ŏ	õ	ŏ		141	-20.14
393	ŏ	311	ŏ	õ	õ			-24.75
394	ŏ	322	ŏ	õ	ō		142	-9.78
395	ŏ	303	õ	õ	õ		143	-7.7
397	õ	347	õ	o			144	-1.58
398				0	0		145	-0.9
	0	362	0	0	0	* OLYMPIC WELL DISCHARGE	146	-2.25
399	0	14	0	0	0	* OLYMPIC WELL	147	-1.35
400	0	343	0	0	0		150	-36.23
401	0	350	0	0	0		151	-1.5
402	0	370	0	0	0		152	-37.21
403	0	372	0	0	0		153	-4.88
404	0	357	0	0	0		154	-1.13
405	0	398	0	0	0		155	-2.63
406	0	390	0	0	0		156	-2.63
407	0	350	0	0	0		158	-0.38
408	0	424.7	0	0	0		159	-1.5
409	0	360	0	0	0		160	-0.75
410	0	445	0	0	0		161	-3.75
411	0	444	Ō	Ō	0		163	-4.13
412	0	420	ō	0	Ō		165	-2.63
413	õ	440	ŏ	õ	õ		167	-1.5
414	õ	447	õ	õ	o		170	
415	ŏ	350	ŏ	ő	õ			-1.5
416	ŏ	358	õ	õ	õ		187	-1.88
417	ŏ	358	õ	ő	õ		190	-0.75
418	ŏ	356	0	0			192	-0.75
419	õ	356			0		193	-1.88
			0	0	0		196	-1.13
420	0	357	0	0	0		200	-2.63
421	0	407	0	0	0		201	-2.63
422	0	380	0	0	0		202	-1.13
423	0	320	0	0	0		203	-3.75
424	0	452	0	0	0		204	-2.25
425	0	455	0	0	0		205	-4.13
426	0	377	0	0	0000		206	-1.13
427	0	354	0	0	0		207	-2.25
428	0	360	D	0	0		208	-38.33
430	0	340	0	0	0		209	-1.13
700	0	332.2	0	0	0		210	-2.63
701	0	330.4	D	0	0		211	-3
702	0	396.4	0	0	0		212	-1.13
703	0	380	0	0	0		214	-1.5
704	0	432.3	0	0	0		215	-1.5
710	0	360	Ō	õ	õ		217	-1.5
DEMAND	S	10000			9.1		219	-3.75
102		-0.45					221	-2.25
103		-2.26					222	-1.43
104		-42.28					223	-1.43
105		-2.6					225	
106		-4.67					225	-1.43
107		-6.42					226	-1.45
108		-20.47					227	-2.29
109		-19.87					221	-6.27
110		-11.78					228	-4.51
111		-34.27					229	-2.26
112							230	-1.58
113		-1.5					231	-1.81
11/		-9.64					232	-1.58
114		-6.62					233	-4.11
115		-5.87					234	-2.29
116		-2.03					235	-3.16
117		-2.48					236	-1.35
118		-2.98					237	-2.26

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240	-2.26	327	-3.08
241	-1.58	329	-3.75
	1.50	770	
242	-1.58	330	-45.12
245	-1.58	331	-5.6
246	-1.81	332	-5.6
		333	
247	-1.81		-8
248	-1.81	334	-1.58
249	-2.26	335	-2.03
250			2.05
250	-2.26	336	-5.87
251	-0.9	337	-3.39
252	-2.26	338	-8.63
253		339	
255	-2.26		-14.19
254	-1.13	340	-3.39
255	-3.53	341	-4.51
254	7 57	342	
256	-3.53		-2.63
257	-3.53	343	-6.48
258	-2.26	344	-19.53
259	-2.26	345	70 7/
	-2.20	343	-30.34
260	-4.29	346	-12.76
261	-1.58	347	-3.02
262	-3.79	348	
	-3.19	340	-1.5
263	-2.29	349	-1.81
264	-1.34	350	-1.81
265	-1.57	351	
			-2.93
266	-1.13	352	-2.48
267	-1.58	353	-3.38
270	-2.29	354	0.00
270	-2.29	334	-2.48
271	-1.81	355	-2.48
272	-1.81	356	-2.93
273		757	2.75
215	-0.45	357	-3.16
274	-2.48	360	-2.03
275	-1.13	361	-2.48
276			2.40
210	-1.13	362	-3.39
277	-2.03	363	-2.48
278	-1.35	364	-2.26
279		3/5	
	-0.45	365	-1.58
280	-2.26	366	-1.81
281	-1.13	367	-4.74
			4./4
282	-2.26	368	-1.81
283	-0.68	369	-8.25
284	-2.93	370	-7.13
205		274	-7.13
285	-2.93	371	-2.63
286	-1.13	372	-9
287	-3.23	373	-5.63
			5.05
290	-5.85	374	-2.33
291	-3	375	-11.09
292	-3	376	-5.26
293	-4.88		
		377	-5.26
295	-7.13	380	-3
296	-1.5	381	-2.63
297			
	-1.5	382	-1.13
299	-0.38	383	-1.88
300	-1.5	385	-3
301	-3.29	387	
			-1.88
302	-4.5	390	-4.13 -
303	-4.88	391	-3.38
304	-1.13	392	-1.5
305	-4.5	393	-1.13
306	-5.03	394	-0.75
307	-1.13	395	-1.13
308	-1.5	397	-2.63
309	-2.03	400	-2.63
310	-2.03	401	-3.38
311	-3.16	402	-3.38
312	-2.26	406	-0.75
313	-5.42	407	-0.75
314			
	-6.77	408	-1.88
315	-5.54	409	-1.5
316	-3.29	410	-36.83
317			
	-3.29	412	-2.25
318	-7.59	414	-4.13
319	-5.6	415	-2.48
320			
	-3.29	416	-1.35
321	-2.25	417	-1.13
323	-2.71	418	-2.48
324			
	-3.84	419	-0.75
325	-2.71	420	-2.26
326	-3.16	421	-0.75
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425 426		-1.13 -1.35					
427		-2.71					
428		-2.48					
FIXED D	EMANDS						
139 -44	.88						
330 -11	.93						
318 -3.	.84						
333 -1.							
399 145		* OLYM	PIC WEL	.L			
425 -10							
AREA DE	MANDS						
MODIFY							
PIPES							
							ICIENCIES
409	339	141	1240	10	135		* UPGRADE ON FRONTAGE RD
515	275	141	1760	10	135		* CREEK & HWY 101 XING
516	251	307	3660	10	135		* CREEK XING SOUTH OF KNOTTS ST.
264	104	262	370	10	135		* UPGRADE TO SUPPORT 101 XING (THOMPSON AVE)
265	262	270	370	10	135		* UPGRADE TO SUPPORT 101 XING (THOMPSON AVE)
273	270	273	480	10	135		* UPGRADE TO SUPPORT 101 XING (THOMPSON AVE)
279	273	274	450	10	135		* UPGRADE TO SUPPORT 101 XING (BEE ST.)
281 318	274 307	275 112	430 200	10 12	135 135		* UPGRADE TO SUPPORT 101 XING (BEE ST.)
510	104	226			2.53.544		* NEW 12" ACROSS 101
221	226	234	410 370	10 10	135 135		* UPGRADE TO SUPPORT 101 XING (THOMPSON AVE) * UPGRADE TO SUPPORT 101 XING (THOMPSON AVE)
232	234	233	70	10	135	*	or deade to sorrow for And (mon son Are)
231	233	247	290	10	135	*	
247	247	246	80	10	135	*	
249	246	248	280	10	135	*	
254	248	251	360	10	135	*	
517	109	345	700	12	135	*	* TEFFT ST. HWY 101 CROSSING
337	135	321	560	8	135	*	
338	321	322	160	8	135	*	
347	322	328	470	8	135	*	* 11 11
348	328	329	360	8	135	*	* 11 11
349	329	330	360	8	135	*	* 11 11
355	333	319	200	8	135	*	* CONCEPCION ST. UPGRADE
356	319	114	900	8	135	*	* " "
519	101	102	5610	12	135	*	* TWIN TANK TEFFT ST. PARALLEL
520	102	103	1560	12	135	*	
521	103	104	510	12	135	*	* 11 11
339	323	322	150	8	135	*	* UPGRADE ON BLACK HAWK WAY
527	187	190	5300	10	135	*	* LOOP ALONG POMEROY
361	345	346	890	10	135	*	* UPGRADE ALONG HILL ST.
528	247	256	700	8	135	*	* LCOP TO INCLUDE NIPOMO EL. SCHOOL
529	326	134	800	8	135		* LCOP-BONITA HOMES TO ORCHARD
464	408	424	1000	10	135	*	
801	199	800	2500	10	135	*	* TIE FROM STANDPIPE TANK TO FRONTAGE RD
713	710	800	3650	10	135	*	* FRONTAGE RD SO OF SUMMIT STATION
NODES							

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603 0 604 0 605 0 606 0 607 0 608 0 609 0 610 0 611 0 612 0 613 0 614 0 615 0 616 0 617 0 618 0 620 0 621 0 622 0 623 0 624 0 625 0 626 0 627 0 628 0 629 0 631 0 632 0 633 0 634 0 635 0 636 0 637 0 644 0 644 0 644 0 644 0	321 -10 320 322 322 330 322 330 311 317 322 335 360 345 360 345 360 360 360 360 360 360 360 360	
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621	-3.76					
626	-1.02					
629	-4.08					
630	-12.19					
631	-6.82					
633	-3.57					
*601	400					
*604	350					
AREA D	EMANDS					
MODIFY						
PIPES						
750	606	750	80	8	135	* TIE IN ON WILLOW RD NEAR BEVINGTON WELL
652	652	751	450	8	125	* TIE NEAR HYDRO TANK
751	631	751	150	8	125	* TIE FROM BARBERRY WAY
752	751	752	80	8	135	* TIE BARBERRY WAY TO WILLOW RD
753	650	652	250	8	135	* HYDROTANK BYPASS
173	175	750	640	10	125	* WILLOW RD TIE IN
754	750	179	490	10	125	* WILLOW RD TIE IN
176	179	752	2700	10	125	* WILLOW RD/BARBERRY WAY TIE IN
527	752	182	2410	10	125	* " " " "
755	187	754	1700	10	135	* POMEROY TIE IN
756	754	753	850	10	135	* 11
757	753	190	2750	10	135	* 11
758	641	753	60	8	135	* "K" ST. TIE IN
759	644	754	60	8	135	* "N" ST. TIE IN
NODES						
750	0	322	0	0	0	
751	0	353	0	0	0	
752	0	353	0	0	0	
753	0	359	0	0	0	
754	0	376	0	0	0	
run	15.27					

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148 152 153 154 154 155 125 226 221 2	146 147 148	151 140 152	140 152 153	440 760 700	10 10 10	125 125 125		224 225	228 229	229 240	370 370	6	125 125
151 155 166 700 10 125 226 222 223 240 250 6 125 153 154 156 60 10 125 233 247 250 6 125 154 158 630 10 125 233 233 233 237 200 6 125 155 159 160 160 10 125 234 235 236 250 6 125 156 164 164 40 10 125 235 235 236 237 70 6 125 164 164 164 150 10 125 236 237 257 256 257 150 6 125 164 164 150 10 125 244 243 242 243 242 243 242 243 244 243 244 243 246 244 243 246 245 246 246 246 246 246<	149	153	154	540	10	125		227	231	241	270	6	125
153 157 158 251 233 247 200 6 125 154 158 159 25 232 233 234 235 234 235 234 235 234 235 234 235 234 235 236<	151	155	168	700	10	125		229	232	242	270		125
154 156 157 252 233 224 70 6 125 158 160 160 60 10 125 233 234 235 236 60 125 158 162 163 60 10 125 235 237 235 237 236 237 236 237 236 237 236 237 250 6 125 164 164 150 10 125 237 256 257 256 267 150 6 125 164 164 150 10 125 238 257 258 257 258 250 8 125 164 170 170 370 16 125 242 241 242 243 242 241 242 243 242 244 243 244 244 244 244 244 244 244 246 246 247 246 246 247 246 246 247 246 <td< td=""><td>153</td><td></td><td></td><td></td><td></td><td>125 125</td><td></td><td>230 231</td><td>232 233</td><td></td><td></td><td>6</td><td>125</td></td<>	153					125 125		230 231	232 233			6	125
156 160 161 40 10 125 224 225 224 227 70 6 125 158 163 164 64 67 10 125 223 234 237 70 6 125 158 164 164 64 67 10 125 223 234 237 236 237 237 6 10 125 237 237 237 6 10 125 237 237 237 6 10 125 237 237 237 8 125 146 10 125 237 237 8 125 136 117 177 136 10 125 242 244	154 155	158	159		10	125		232	233	234	70	6	125
158 162 163 80 10 125 233 235 236 600 6 125 160 164 165 240 10 125 237 255 256 600 6 125 164 164 165 100 125 238 225 257 150 6 125 164 167 170 370 10 125 244 244 241 241 242 240 6 125 164 170 171 2160 16 125 244 246 246	156	160	161	40	10	125		234	235	236	550	6	125
19-9 18-2 18-2 27 255 256 600 6 125 164 166 166 166 166 167 160 165 2239 2257 150 16 125 164 166 167 170 370 10 125 224 224 224 224 224 224 226 28 370 8 125 164 177 170 370 10 125 224	158	162	163	80	10	125		236	236 237	255		6	125 125
161 165 166 150 10 125 229 257 258 370 8 125 163 167 170 370 10 125 240 240 224 221 421 421 424 242 421 424 424 423 424 </td <td>160</td> <td></td> <td></td> <td></td> <td></td> <td>125 125</td> <td></td> <td>237 238</td> <td>255 255</td> <td>256 257</td> <td>600</td> <td>6</td> <td>125</td>	160					125 125		237 238	255 255	256 257	600	6	125
163 167 170 370 10 125 241 258 250 370 8 125 164 170 171 2160 16 125 242 242 242 242 242 242 242 244 243 80 8 125 164 172 174 1800 16 125 244 243 244 243 244 <td></td> <td></td> <td>166</td> <td></td> <td>10</td> <td>125</td> <td></td> <td>239</td> <td>257</td> <td>258</td> <td>520</td> <td>8</td> <td>125</td>			166		10	125		239	257	258	520	8	125
165 171 172 3550 16 125 243 242 243 244 243 89 8 125 1667 173 174 1700 12 125 244 243 244 243 80 8 125 1667 173 174 1700 10 125 244 244 244 247 246 247 80 8 125 166 174 175 900 10 125 246 247 246 247 80 8 125 177 176 175 170 100 125 251 248 249 249 80 8 125 176 177 181 180 335.2 8 125 251 251 251 430 8 125 177 183 184 377 8 125 256 252 254 430 8 125 178 183 184 126 8 125 256 252<	163	167	170	370	10	125		241	258	250	370	8	125
166 172 173 1800 16 125 244 244 243 288 89 8 125 168 174 175 900 10 125 246 242 248 248 244 248 246 247 80 8 125 168 174 177 900 10 125 246 247 248 244 248 248 247 80 8 125 177 176 176 10 125 251 249 250 8 125 177 176 179 100 125 252 251 249 250 8 125 176 179 182 510 10 125 254 251 430 8 125 177 185 184 357 8 125 251 251 252 253 500 8 125 177 185 184 183 180 125 256 251 252 253 </td <td>165</td> <td>171</td> <td>172</td> <td>3650</td> <td>16</td> <td>125</td> <td></td> <td>242 243</td> <td>241 242</td> <td>242 218</td> <td></td> <td></td> <td>125 125</td>	165	171	172	3650	16	125		242 243	241 242	242 218			125 125
168 174 175 900 10 125 246 242 245 380 6 125 170 178 177 198 10 125 247 248 247 249 880 8 125 171 177 178 177 178 177 178 177 178 177 178 177 178 177 179 1130 10 125 249 249 250 248 249 520 8 125 174 181 180 335.2 8 125 251 245 249 251 650 8 125 176 187 184 5110 10 125 254 244 251 430 8 125 178 184 181 183 120 8 125 251 252 252 259 537 6 125 178 184 191 140 8 125 259 259 255 1370 6 1	166 167		173 174			125 125		244	244	243	89	8	125
	168	174	175	900	10	125		246	242	245	380	6	125
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	170	178	177	198	10	125		248	247	249	880	8	125
	171 172					125 125		249 250	246 248	248 249	280 520	8 8	125 125
176 179 120 10 125 253 250 254 248 350 8 125 177 185 184 357 8 125 255 255 251 252 400 8 125 178 184 183 182 10 8 125 256 252 259 120 8 125 180 185 187 1260 8 125 256 259 120 8 125 181 186 1260 8 125 260 259 255 370 6 125 183 190 191 40 8 125 261 260 103 370 6 125 184 191 192 193 1130 10 125 264 262 104 370 8 125 185 192 193 3150 10 125 266 262 270 370 8 125 186 194 196	173	175	179			125		251	249	219	650	8	125
177 185 184 357 8 125 255 251 252 490 8 125 178 184 183 182 10 8 125 257 253 254 460 8 125 180 183 186 1260 8 125 257 259 120 8 125 181 183 186 1260 8 125 260 259 256 370 6 125 183 190 191 40 8 125 261 260 103 370 6 125 184 191 192 193 1130 10 125 264 262 104 370 8 125 186 192 193 3516 10 125 266 262 270 370 8 125 187 194 196 950 10 125 266 262 263 460 6 125 199 196 100	175	180	179	200	10	125		253	250	254	350	8	125
178 184 183 250 8 125 256 252 253 590 8 125 180 183 187 1260 8 125 257 252 254 460 8 125 180 183 186 1260 8 125 259 259 259 257 253 254 460 8 125 181 183 186 1260 8 125 266 260 103 370 6 125 184 191 192 870 8 125 264 260 261 260 261 260 61 125 185 192 193 1360 10 125 264 262 270 370 8 125 186 194 196 950 10 125 266 262 263 264 430 6 125 190 201 203 540 100 125 276 270 265 264 520	177	179	184	357	8	125		254 255	248 251	251 252	430 490		125 125
180 183 187 1260 8 125 258 152 259 1520 8 125 181 183 186 125 260 259 255 370 6 125 182 393 395 1350 8 125 260 259 265 370 6 125 184 191 192 870 8 125 264 265 264 265 264 265 264 265 264 265 264 252 264 264 264 265 264 252 264 264 264 266 266 266 266	178 179		183 182		8 8	125 125		256	252	253	590	8	125
182 393 395 1350 8 125 260 259 265 370 6 125 184 190 191 40 8 125 261 260 103 370 6 125 184 191 192 870 8 125 262 260 251 300 6 125 186 192 193 316 10 125 264 262 104 370 8 125 187 194 195 3400 8 125 266 262 270 370 6 125 189 196 197 500 10 125 266 262 264 430 6 125 190 201 203 1800 10 125 268 264 227 370 6 125 197 203 204 650 10 125 270 226 266 60 125 194 204 205 330 8	180	183	187	1260	8	125		258	102	259	1320	8	125
1841911928708125262260261300612518519219311301252632642621043708125187194195348081252642621043708125187194195348081252662622634506125188194196950101252662622634506125189196197500101252662632644306125190201500101252692642723706125192202203540101252702712652665206125194204205330812527327027348081251952062079008125276271274480612519820820981081252772744806125200210211370812527727127448061252012113708125280274277470612520221221314708125280274277	182	393	395	1350	8	125		260	259	265	370		125
185 192 193 1130 10 125 263 261 262 200 6 125 186 193 198 3516 10 125 264 262 104 370 8 125 187 194 195 3480 8 125 265 262 263 271 370 8 125 188 194 196 950 10 125 266 262 263 271 370 6 125 190 200 201 500 10 125 266 264 272 370 6 125 193 203 204 650 10 125 270 265 266 520 6 125 194 204 205 330 8 125 271 270 271 450 6 125 195 206 207 900 8 125 276 271 274 480 6 125 196 206 <td></td> <td></td> <td></td> <td></td> <td></td> <td>125 125</td> <td></td> <td>261 262</td> <td>260 260</td> <td>103</td> <td></td> <td></td> <td>125</td>						125 125		261 262	260 260	103			125
	185	192	193	1130	10	125		263	261	262	200	6	125
189 196 197 500 10 125 267 263 271 370 6 125 190 200 201 500 10 125 268 264 272 370 6 125 191 201 203 1800 10 125 269 264 272 370 6 125 192 202 203 540 10 125 270 265 266 520 6 125 194 204 205 330 8 125 272 267 270 620 6 125 196 206 60 8 125 274 270 271 480 8 125 197 207 208 209 810 8 125 276 271 274 480 6 125 200 210 211 370 8 125 276 271 274 450 6 125 201 211 170 8	187	194	195	3480	8	125		265	262	270	370	8	125
190 200 201 500 10 125 268 263 264 430 6 125 191 201 203 1400 10 125 269 264 272 370 6 125 193 203 204 650 10 125 270 265 266 520 6 125 194 204 205 330 8 125 271 265 266 6 8 125 196 206 207 900 8 125 273 270 271 450 6 125 197 207 208 20 8 125 276 271 274 480 6 125 198 208 209 810 8 125 276 271 274 480 6 125 200 210 211 370 8 125 278 273 276 470 6 125 201 211 214 1450						125		266 267		263 271			125 125
$\begin{array}{cccccccccccccccccccccccccccccccccccc$						125 125		268	263	264	430	6	125
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	192	202	203	540	10	125		270	265	266	520	6	125
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	194	204	205	330	8	125							
$\begin{array}{cccccccccccccccccccccccccccccccccccc$													125
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	197	207	208	20	8	125		275	271	274	480	6	125
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	199	209	210	80	8	125		277	272	275	480		125
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	201		212	330		125 125							125 125
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	202	212	213		8	125		280	274	277	470	6	125
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	204	214	215	1070	8	125		282	275	278	470	6	125
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	206	216	217	130	8	125				279			
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	207 208					125 125						6	125
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	209	220	221	910	10	125		287	279	283	450	8	125
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	211	107	222	440	8	125		289	280	282	480		125
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	213	222 222	223 230			125 125		290 291					125
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	214	223	230	430	6	125		292	113	284	780	6	125
21822522645061252962852863006125219225232440612529728628711061252202262275206125298287290198061252212262343706125299290291250612522222722852061253002912925306125	216	224	225	430	6	125		294	284	268	340	6	125
219225232440612529728628711061252202262275206125298287290198061252212262343706125299290291250612522222722852061253002912925306125	218	225	226	450	6	125		296	285	286			125
221 226 234 370 6 125 299 290 291 250 6 125 222 227 228 520 6 125 300 291 292 530 6 125	220	226	227			125		297	286	287	110	6	125
	221	226	234	370	6	125		299	290	291	250	6	125
	223												

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302	293	294	200	6	125		380	360	361	400	6	125
303	294	295	510	6	125		381	360	362	260	6	125
304	295	296	530	6	125							125
					125		382	362	363	400	6	125
305	296	297	860	6	125		383	362	364	660	6	125
306	297	298	1000	6	125		384	357	356	260	6	125
307	298	299	200	6	125		385	356	361	280		125
308	299	300	300		125		305	350			6	125
				8	125		386	361	363	260	6	125
309	300	301	540	8	125		387	363	364	260	6	125
310	301	118	480	8	125		388	150	357	150	6	125
311	299	302	770	6	125		389					
312					125		309	145	364	150	6	125
	302	303	560	6	125		390	353	369	680	6	125
313	303	304	400	6	125		391	144	365	140	6	125
314	303	269	450	6	125		392	365	367	640	6	125
315	269	304	830	6	125		393	7/5			2	125
					125		242	365	366	260	6	125
316	304	305	380	6	125		394	366	367	370	6	125
317	305	306	780	6	125		395	366	368	260	6	125
318	112	307	200	8	125		396	367	368	640	6	125
319	307	308	500		125		370	307	300			125
				8	125		397	143	368	140	6	125
320	306	310	520	6	125		398	153	370	1800	6	125
321	310	309	300	6	125		399	369	370	380	6	125
322	309	116	570	6	125		400	221	371	570		125
323		711			125		400	221	371		8	125
	121	311	520	6	125		401	371	372	1000	8	125
324	311	312	670	6	125		402	372	373	1620	8	125
325	312	122	200	6	125		403	373	374	280	8	125
326	123	313	300	6	125		101	77/	775		č	125
		313			125		404	374	375	310	8	125
327	313	314	630	6	125		405	375	376	650	8	125
328	126	314	540	6	125		406	374	377	650	8	125
329	127	315	590	6	125		407	376	377		8	125
								3/6	311	230	•	125
330	131	315	340	6	125		408	376	339	800	6	125
331	315	316	160	6	125		409	339	141	1240	6	125
332	316	317	675	6	125		410	155	380	850	6	125
333	316	320	760	6	125		410	100				125
							411	220	380	390	6	125
334	317	320	180	6	125		412	380	381	940	6	125
335	320	133	398	6	125		413	381	157	760	6	125
336	320	301	500	6	125		414	381	203			105
	175	701	540				414	201	205	750	6	125
337	135	321	560	6	125		415	381	382	640	6	125
338	321	322	160	6	125		416	382	158	770	6	125
339	322	323	150	6	125		417	382	383	370	6	125
340	323	324	260	8	125		411	302				125
		324		0			418	383	204	380	6	125
341	324	326	430	8	125		419	383	206	780	6	125
342	323	325	440	8	125		420	163	384	450	6	125
343	325	326	260	8	125		421	384	385	320	6	125
344	325	327	210		125		461	304	305		0	123
		321		8	125		422	385	386	600	6	125
345	327	132	930	8	125		423	386	208	170	6	125
346	327	130	980	8	125		424	165	378	590	6	125
347	322	328	470	6	125		125					125
							425	378	387	210	8	125
348	328	329	360	6	125		426	387	388	600	8	125
349	329	330	360	6	125		427	388	210	350	8	125
350	330	331	1020	8	125		428	170	389	180	8	125
351	331	332	360		125							
331		332		8	125		429	389	390	430	8	125
352	332	333	210	8	125		430	390	391	590	8	125
353	332	318	800	6	125		431	391	212	310	8	125
354	318	116	550	6	125		432	160	392	720	~	105
355		710			125				392	720	6	125
	333	319	200	6	125		433	163	393	780	8	125
356	319	114	900	6	125		434	165	394	620	8	125
357	138	342	660	8	125		435	394	395	550	8	125
358	342	343	330	8	125		436	209	397	1210	2	125
359	343	344	1220	š	125		430	209			6	125
		344		8	125		437	397	400	600	8	125
360	344	345	820	8	125		438	400	207	980	6	125
361	345	346	890	8	125		439	400	401	910	8	125
362	346	347	900	6	125						~	105
363		770			125		440	401	205	980	6	125
	346	338	420	8	125		441	401	201	510	10	125
364	338	347	600	8	125		442	397	402	420	10	125
365	347	330	1970	8	125		443	402	217	470	8	125
366	152	348	520	6	125		445					125
367	348	7/0	170		125		444	402	200	1660	10	125
		349	170	6	125		445	190	403	2530	8	125
368	349	350	270	6	125		446	403	404	1230	8	125
369	349	351	600	6	125		447	404	407			125
370	350	351	410		125		441			2150	8	125
370		331		6	125		448	404	405	1020	8	125
371	351	352	560	6	125		449	405	406	390	8	125
372	350	352	220	6	125		450	406	407	1270	8	125
373	352	151	130	6	125						0	125
374	7/0	757		~	105		451	406	408	1100	8	125
5/4	348	353	860	6	125		452	405	410	3700	8	125
375	353	354	200	6	125		453	408	409	3260	8	125
376	354	357	950	6	125		454	192	411	1630	в	125
377	354	355	150	6	125							
770	755	75/			125		455	411	410	80	8	125
378	355	356	600	6	125		456	410	409	1600	8	125
379	355	360	260	6	125		457	411	412	950	8	125
							2335202	1000			1000	

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150			750	-		
458	412	413	350	8	125	
459	412	430	1030	8	125	
460 461	414 191	193 421	1730 1120	8	125 125	
462	403	422	560	8 8	125	
463	407	423	670	8	125	
464	408	424	1000	8	125	
465	414	425	480	8	125	
466	147	420	590	6	125	
467	420	419	380	6	125	
468	419	139	570	6	125	
469	146	416	640	6	125	
470	416	417	40	6	125	
471	417	418	330	6	125	
472	418	419	300	6	125	
473	417	415	220	6	125	
474	415	343	470	6	125	
475	418	342	690	8	125	
476	125	334	180	6	125	
477	334	335	440	6	125	
478	334	336	250	6	125	
479	336	337	700	6	125	
480 481	124 335	335	150 290	6	125	
482	427	427 337	230	6	125 125	
482	337	426	440	6	125	
484	427	428	440	6	125	
485	426	428	220	6	125	
486	428	122	400	6	125	
487	426	340	240	6	125	
488	340	120	570	6	125	
489	340	341	580	6	125	
490	341	117	290	6	125	
491	399	398	348	8	125	
492	398	385	200	8	125	
493	169	174	332	8	125	
501	133	132	400	10	125	
505	168	156	700	10	125	
506	156	168	750	6	125	
507	194	198	2084	12	125	
508	198	199	2049	16	125	
509	159	392	1642	6	125	
510 511	104 103	226 227	410 410	8	125	
512	105	224	410	6	125 125	
513	409	430	1100	8	125	* DALE AVE
514	430	414	4460	8	125	* FRISCO WAY
* THIS	IS THE		LAKE SYSTEM	Ŭ	100	TRIBCO MAT
601	601	602	355	8	125	* BLACK LAKE
602	602	603	250	8	125	
603	604	605	330	8	125	* BLACK LAKE
604	605	603	50	8	125	
605	603	606	90	10	125	
606	606	607	1030	8	125	
607	607	608	770	8	125	
608	608	609	350	8	125	
609	608	613	620	8	125	
610 611	607 610	610 611	340 400	8 8	125 125	
612	610	611	840	8	125	
613	611	612	220	8	125	
614	612	613	220	8	125	
615	612	614	730	8	125	
616	613	614	980	8	125	
617	614	615	180	8	125	
618	616	617	80	8	125	
619	616	619	1080	8	125	
620	620	621	60	8	125	
621	621	622	280	8	125	
622	621	623	950	8	125	
623	623	624	60	8	125	
624	624	625	50	8	125	
625	625	626	270	8	125	
626 627	616 627	627 626	800 320	8	125 125	
628	626	628	600	8	125	
629	627	629	330	8	125	
630	628	629	530	8	125	

LAKE #4 LAKE #3 .

631 632 633 634 635 636 637 641 642 643 644 645 644 645 644 645 644 645 651 652 653 654 NODES	628 629 618 606 631 630 633 633 633 633 633 633 640 642 642 641 642 641 652 651 652 652 619 609	630 618 631 632 631 633 634 635 634 635 634 637 640 641 642 643 644 651 651 652 618 631 620 619	360 250 610 3340 200 650 570 400 450 350 1180 1380 1040 830 245 720 930 2600 170 170 710 600 1100 450	888888888888888888888888888888888888888	125 125 125 125 125 125 125 125 125 125
101 101 103 104 105 1067 109 1101 103 104 105 1067 109 111 112 113 114 115 117 118 119 111 111 112 123 124 125 126 127 128 129 121 1223 123 123 123 123 131 132 1334 134 142 144 144 144 144 144 144 144 144 144 144 144	000000000000000000000000000000000000000	523.8 360 342 336 329 324 316 320 328 331 310 333 343 350 351 357 329 356 343 337 337 337 337 326 343 337 326 343 337 326 343 337 326 343 337 326 343 357 367 373 356 357 367 373 356 357 367 373 356 357 367 373 356 357 367 373 356 357 367 373 356 357 367 373 356 357 367 376 357 376 355 367 377 376 356 357 367 377 376 356 357 367 377 376 356 367 377 376 356 367 377 376 356 367 377 376 356 367 377 376 356 367 377 376 356 367 377 376 356 367 377 376 357 356 367 377 356 367 377 376 357 367 377 376 357 367 377 356 367 377 376 357 356 367 377 376 357 356 367 377 376 357 356 367 377 376 357 356 357 367 377 356 357 356 357 356 367 377 356 357 356 367 377 356 357 367 356 367 373 356 367 373 356 367 373 356 367 373 356 367 372 356 360 374 362 350 361 343 320	000000000000000000000000000000000000000	000000000000000000000000000000000000000	000000000000000000000000000000000000000

*OLD DEDICATED WELL LINE

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* OLD HYDRO TANK

159	0	330	0	0	0		
160	Ō	340	ō	ŏ	ŏ		
161	0	340	0	0	0		
162	0	340	0	0	0		
163	0	340	0	0	0		
164	0	340	0	0	0		
165	0	335	0	0	0		
166	0	330	0	0	0		
167 168	0	315 340	0	0	0		
169	õ	-65.6	ō	0	0		VIA CONCHA WELL
170	ŏ	306.4	ŏ	õ	0		VIA CONCHA WELL
171	ŏ	305	ŏ	ŏ	ō		
172	ŏ	225	ŏ	ŏ	õ		
173	ō	254	ŏ	ŏ	ŏ		
174	0	267	õ	õ	õ	*	VIA CONCHA WELL DISCHARGE
175	0	283	0	0	D		
176	0	283	0	0	0		
177	0	183	0	0	0	*	EUREKA WELL DISCHARGE
178	0	- 15	0	0	0	*	EUREKA WELL
179	0	322	0	0	0		
180	0	325	0	0	0		BEVINGTON WELL DISCHARGE
181	0	-10.2	0	0	0	*	BEVINGTON WELL
182	0	394	0	0	0		
183 184	0	394	0	0	0		
185	ö	380 23	0	0	0		OMIYA WELL DISCHARGE OMIYA WELL
186	õ	362	õ	0	0		UMITA WELL
187	ŏ	362	ŏ	õ	õ		
190	ŏ	410	ŏ	ŏ	õ		
191	ŏ	410	õ	õ	ŏ		
192	õ	430	õ	ŏ	ŏ		
193	Ō	428	ō	õ	ŏ		
194	0	404	0	Ō	Ō		
195	0	410	0	0	0		
196	0	380	0	0	0		
197	0	367	0	0	0		
198	0	400	0	0	0		
199	0	459.63	0	0	0	*	STANDPIPE TANK
200	0	370	0	0	0		
201	0	357	0	0	0		
202	0	357	0	0	0		
203	0	343	0	0	0		
204 205	0	340 347	0	0	0		
205	0	347	0	0	0		
207	ŏ	345	ŏ	õ	ō		
208	ŏ	345	ŏ	õ	õ		
209	ŏ	330	ŏ	ŏ	ŏ		
210	õ	328	ŏ	ŏ	õ		
211	Ō	327	Õ	ŏ	ŏ		
212	0	325	0	0	Ō		
213	0	336	0	0	0		
214	0	361	0	0	0		
215	0	370	0	0	0		
216 217	0	359	0	0	0		
217	0	359	0	0	0		
218	0	313	0	0	0		
219	0	350	0	0	0		
220 221	0	360 368	0	0	0		
222	0	317	0	0	0		
223	õ	317	0	õ	0		
224	õ	317	0	0	0		
225	õ	319	õ	ŏ	õ		
226	õ	325	ŏ	ŏ	õ		
227	0	331	0	0	õ		
228	0 0 0	337	0	0	0		
229	0	347	0	0	0		
230	0	307	0	0	0		
231	0	311	0	0	0		
232	0	315	0	0	0		
233	0	321	0	0	0		
234	0	321	0	0	0		
235 236	0	327 337	0	0	0		
237	õ	338	0	o	ŏ		
240	ŏ	361	ŏ	õ	õ		
			20	-			

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* CHURCH WELL DISCHARGE * CHURCH WELL .

704			•	•			107				
321 322	0	397 398	0	0	0				72 0		0
323	ŏ	404	ö	ő	0				57 0 98 0		0
324	ŏ	397	õ	ŏ	0				90 0		0
325	ŏ	398	ŏ	ŏ	ŏ				50 0		ő
326	õ	399	ŏ	ŏ	õ				24.7 0		ő
327	ō	362	ŏ	õ	õ				60 0		õ
328	0	397	0	ŏ	ō	14.			45 0		ŏ
329	0	358	0	ō	õ				44 0		ō
330	0	354	0	ō	ō				20 0		Ō
331	0	344	0	Ō	0		413		40 0		0
332	0	340	0	0	0		414	0 4	47 0		0
333	0	337	0	0	0			0 3	50 0	0	0
334	0	337	0	0	0				58 0	0	0
335	0	340	0	0	0				58 0	0	0
336	0	347	0	0	0				56 0		0
337	0	350	0	0	0			0 3	56 0		0
338	0	342	0	0	0				57 0		0
339	0	360	0	0	٥				07 0		0
340	0	374	0	0	0				80 0		0
341	0	364	0	0	0			0 3	20 0		0
342	0	326	0	0	0				52 0		0
343	0	320	0	0	0				55 0		0
344	0	350	0	0	0				77 0		0
345	0	360	0	0	0				54 0		0
346	0	360	0	0	0				60 0		0
347	0	353	0	0	0			0 3	40 0		0
348 349	0	372	0	0	0		* THIS I	S THE BLA	CK LAKE		
350	ő	371 362	0	0	0				38 0		0
351	ŏ	342	0	0	0				17 0		0
352	o	361	Ö	0	0				21 0		0
353	ŏ	361	ŏ	ő	0				10 0		0
354	õ	370	ö	0	0				20 0 22 0		0
355	ŏ	387	ŏ	0	0						0
356	ő	360	õ	0					22 0 30 0		0
357	ŏ	360	ŏ	ő	0				28 0		0
360	õ	401	ō	ö	o				30 0		0
361	õ	374	õ	ő	õ				11 0		0
362	ŏ	408	ŏ	ő	ő				17 0		0
363	ŏ	372	ŏ	ŏ	ŏ				22 0		0
364	ŏ	370	ŏ	õ	o			0 3	35 0		0
365	õ	370	ŏ	õ	ō				50 0		
366	ŏ	370	ŏ	ö	õ				60 0		0 C
367	õ	400	ŏ	ŏ	ŏ				60 0		c
368	ŏ	381	ŏ	õ	õ				45 0		C O
369	ō	348	ō	ō	õ				28 0		ō
370	õ	358	õ	õ	õ				60 0		č
371	ō	380	ō	õ	ō				61 0		č
372	õ	389	õ	õ	õ				62 0		ò
373	ō	360	õ	ō	õ				69 0		õ
374	0	360	0	0	0				70 0		c
375	õ	360	0	õ	õ				74 0	100	č
376	0	360	0	0	Ō				62 0		č
377	0	360	0	0	Ō				45 0		ò
378	0	380	0	0	0				63 0		Ō
380	0	380	0	0	0				50 0		(
381	0	360	0	0	0				65 0	0	(
382	0	369	0	0	0		631	0 3	53 0	0	0
383	0	360	0	0	0		632		61 0		0
384	0	340	0	0	0		633	0 3	62 0	0	C
385	0	359	0	0	0			0 3	81 0	0	(
386	0	320	0	0	0		635	0 3	41 0	0	(
387	0	342	0	0	0		636	0 3	52 0	0	0
388	0	317	0	0	0		637	0 3	84 0	0	0
389	0	317	0	0	0				80 08		(
390	0	339	0	0	0				59 0		ſ
391	0	316	0	0	0				73 0		ú
392	0	317	0	0	0				81 0	6 (B)	0
393	0	311	0	0	0				76 0		r
394	0	322	0	0	0				20 0		1
395	0	303	0	0	0				30 0		1
397	0	347	0	0	0			0 3	60 0	0	0
398	0	362	0	0	0	* OLYMPIC WELL DISCHARGE	DEMANDS				
399	0	14	0	0	0	* OLYMPIC WELL	102		2.48		
400	0	343	0	0	0		103		2.71		
401	0	350	0	0	0		104			INCS JOCK	os
402	0	370	0	0	U		105	5	3.02		
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106	-5.08	211	-3.75
107	-10.85	212	-1.13
108	-23.6 * INCS LAUNDROMAT	213	-10.13
109	-28.62 * INCS BUENA VISTA MHP	214	-1.5
110	-23.47		
		215	-1.5
111	-26.64 *INCS BAR K MHP USAGE AND CHURCH	217	-1.5
112	-3.0	219	-3.75
113	-7.12 * INCS APTS ON AMADO	221	-2.25
114	-8.43	222	-1.55
115	-5.87	223	-1.43
116	-2.03		
117		224	-1.43
	-2.48	225	-1.93
118	-2.98	226	-2.29
120	-1.58	227	-6.27
121	-1.81	228	-4.74
122	-2.48	229	-2.26
123	-1.81	230	-1.58
124	-1.58	231	-2.03
125	-1.35		
		232	-1.58
126	-1.81	233	-2.37 * INCS ST. JOSEPHS CHURCH
127	-2.26	234	-2.29
130	-3.38	235	-3.16
131	-1.35	236	-1.35
132	-1.5	237	-2.26
133	-5.36		
		240	-2.26
134	-8.41	241	-1.58
135	-6.75	242	-3.38
136	-7.13	245	-1.58
137	-4.58 * NEED TO ADD DANA ELEM SCHOOL DEMAND	246	-3.84
138	-1.95	247	-1.81
139	-2.25		
141	-35.98 * INCS SWAP MEET	248	-4.06
	-33.90 - INCS SWAP MEET	249	-5.26 * +3 GPM IRRIG
142	-4.58 * NEED TO ADD DANA ELEM SCHOOL DEMAND -1.95 -2.25 -35.98 * INCS SWAP MEET -11.37 -7.7 -1.58	250	-2.26
143	-7.7	251	-4.06
144	-1.58	252	-9.03
145	-0.9	253	-9.03
146	-2.63	254	-4.29
147	-1.35	255	-4.43
150	-0.9		
		256	-3.53
151	-1.5	257	-3.53
152	-1.88	258	-2.26
153	-4.88	259	-2.26
154	-4.13 * +3 GPM IRRIG	260	-4.29
155	-2.63	261	-1.58
156	-4.16	262	-5.37
157	-2.33		
		263	-5.00
158	-1.33	264	-3.35
159	-3.04	265	-3.15
160	-2.25	266	-1.13
161	-3.75	267	-3.61
163	-4.88	270	-3.19
165	-2.63	271	-2.03
166	-1.33		
167	- (272	-1.81
107	-4.88	273	-1.35
170	-6.0	274	-3.16
171	-16.13	275	-2.63
172	-10.88	276	-2.03
173	-10.13	277	-3.84
175	-13.13	278	-4.88
183	-10.13	279	-0.45
187	-4.69	280	
190		280	-2.26
	-7.65	281	-2.63
192	-2.25	282	-2.26
193	-6.94	283	-0.68
194	-7.99	284	-2.93
195	-23.4	285	-2.93
196	-1.13	286	-2.40
200	-7.58	287	-6.74
201	-7.50		
202	-4.00	290	-9.17
	-6.00	291	-3
203	-3.75	292	-5.26
204	-2.25	293	-7.81
205	-4.13	295	-8.70
206	-1.13	296	-4.43
207	-2.25	297	-3.68
208	-3.00	298	-0.75
209	-1.13	299	-1.50
210	-2.63	300	-1.5
		500	

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704	7	
301	-3.29	387 -1.88
302	-5.10	390 -4.13
303	-6.91	391 -3.38
304	-1.13	392 -6.38
305	-5.25	393 -3.38
306	-5.03	394 -4.50 *+3 GPM IRRIG
307	-1.13	395 -1.50
308	-14.14	397 -2.63
309	-2.03	그는 것 같아요. 이 것 않아요. 이 집 않아요. 이 것 않아요. 이 것 않아요. 이 집 않아요. 이
310	-2.03	399 0 *OLYMPIC WELL DISCHARGE 400 -2.63
311	-3.53	
312	-2.26	401 -4.88
313	-5.42	402 -3.38
314	-5.42	403 -5.44
315	-5.54	405 -2.63
316		404 -2.06
	-3.29	406 -1.13
317	-3.29	407 -1.95
318	-7.59	408 -5.63
319	-7.54	409 -6.00
320	-3.29	410 -2.25
321	-3.25 * +3 GPM IRRIG	411 -1.88
323	-2.71	413 -3.75 * +3 GPM IRRIG
324	-3.84	412 -2.25
325	-2.71	414 -6.38
326	-3.16	415 -2.48
327	-3.08	416 -1.35
329	-3.75	417 -1.13
330	-39.86	
331	-6.9	
332	-10.06	419 -0.75
333	-6.73	420 -2.26
334		421 -0.75
	-1.58	422 -1.13
335	-2.03	423 -1.2
336	-5.87	424 -1.61
337	-3.39	425 -1.13
338	-12.80	426 -1.35
339	-33.71	427 -2.71
340	-3.39	428 -2.48
341	-4.51	* THIS IS THE BLAKE LAKE SYSTEM
342	-3.75	606 -3.82
343	-6.48	607 -7.65
344	-23.44	608 -7.65
345	-21.87 * INCS VONS AND BANK	609 -1.91
346	-6.59 * INCS RECREATION USAGE	
347	-3.02	610 -4.7B
348	-1.88	611 -4.14
349	-1.81	612 -4.46
350		613 -6.69
	-2.18	614 -10.84
351	-2.93	616 -2.87
352	-2.48	625 -3.19
353	-3.38	626 -1.91
354	-2.48	627 -4.46
355	-2.48	628 -6.05
356	-2.93	629 -5.42
357	-3.16	630 -4.46
360	-2.03	631 -5.74
361	-2.48	633 -3.06
362	-3.39	634 -2.29
363	-2.48	635 -2.29
364	-2.26	637 -8.60
365	-1.58	
366	-1.81	640 -4.78
367	-4.74	641 -2.87
368	-1.81	642 -1.91
369		643 -4.14
370	-9.00	FIXED DEMANDS
	-7.13	139 -23.88 * NIPOMO REGIONAL PARK
371	-2.63	330 -9.19 * NURSERY ON GRANDE
372	- 13.95	318 -2.47 * LANDSCAPE METER
373	-5.63	333 -1.27 * GRANDE APTS LANDSCAPE METER
374	-2.33	604 350 * BLACK LAKE WELL #3
375		* THIS IS THE BLACK LAKE IRRIGATION DEMANDS
77/	-8.48 * INCS COMMERCIAL USAGE	
376	-5.26	
377		606 -1.65
	-5.26	606 -1.65 607 -0.58
377	-5.26 -5.26	606 -1.65 607 -0.58 608 -1.65
377 380 381	-5.26 -5.26 -3	606 -1.65 607 -0.58 608 -1.65 609 -0.89
377 380 381 382	-5.26 -5.26 -3 -2.63 -2.63	606 -1.65 607 -0.58 608 -1.65 609 -0.89 614 -0.34
377 380 381 382 383	-5.26 -5.26 -3 -2.63 -2.63 -1.88	606 -1.65 607 -0.58 608 -1.65 609 -0.89 614 -0.34 615 -1.88
377 380 381 382	-5.26 -5.26 -3 -2.63 -2.63	606 -1.65 607 -0.58 608 -1.65 609 -0.89 614 -0.34 615 -1.88 616 -10.67

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618 621 626 629 630 631 633 *99 14 237 AREA DI MODIFY PIPES	-3000		YMPIC WELL RE FLOW			
		S NEE	DED TO MEET	EXI	STING SYSTEM	DEFICIENCIES.
409	339	141	1240	10	135	* UPGRADE ON FRONTAGE RD
515 516	275 251	141 703	1760	10	135	* CREEK & HWY 101 XING
264	104	262	2660 370	10 10	135 135	* CREEK XING SOUTH OF KNOTTS ST. * NEW 10" ACROSS 101
265	262	270	370	10	135	* NEW 10" ACROSS 101
273 279	270 273	273 274	480 450	10 10	135 135	* NEW 10" ACROSS 101
281	274	275	430	10	135	* NEW 10" ACROSS 101 * NEW 10" ACROSS 101
318	307	112	200	12	135	* NEW 12" ACROSS 101
510	104	226	410	10	135	* NEW 10" ACROSS 101
221 232	226 234	234 233	370 70	10 10	135 135	* NEW 101 10" * NEW 101 10" " "
231	233	247	290	10	135	* NEW 101 10" " "
247	247	246	80	10	135	* NEW 101 10" " "
249 254	246 248	248 251	280 360	10 10	135 135	* NEW 101 10"" " " * NEW 101 10" " " "
517	109	345	700	10	135	* TEFFT ST. HWY 101 CROSSING
337	135	321	560	8	135	* GRANDE AVE UPGRADE
338 347	321 322	322 328	160 470	8 8	135 135	* GRANDE AVE UPGRADE * GRANDE AVE UPGRADE
348	328	329	360	8	135	* GRANDE AVE UPGRADE
349	329	330	360	8	135	* GRANDE AVE UPGRADE
355 356	333 319	319 114	200 900	8 8	135 135	* CONCEPCION ST. UPGRADE * CONCEPCION ST UPGRADE
519	101	102	5610	12	135	* TWIN TANK TEFFT ST. PARALLEL
520	102	702	400	12	135	* NEW TANK LINE
521 339	103 323	104 322	510 150	12 8	135 135	* NEW TANK LINE * UPGRADE ON BLACK HAWK WAY
527	187	190	5300	10	135	* LOOP ALONG POMEROY
361	345	346	890	10	135	* UPGRADE ALONG HILL ST.
528 529	247 326	256 134	700 800	8 8	135 135	* LOOP TO INCLUDE NIPOMO EL. SCHOOL * LOOP-BONITA HOMES TO ORCHARD
464	408	424	1000	10	135	* POPPEY LANE UPGRADE
801	199	800	2500	10	135	* TIE FROM STANDPIPE TANK TO FRONTAGE RD
713 *THESE	710	800	3650	10	135 SYSTEM DEMAND	* FRONTAGE RD SO OF SUMMIT STATION
700	141	345	1400	8	135	*FRONTAGE RD JUNIPER TO TEFFT
701	273	700	1750	8	135	*LEAF ST THOMPSON TO CEDARWOOD
702 703	700 266	266 701	730 370	8 8	135 135	*CEDARWOOD
704	701	702	370	8	135	*CEDARWOOD *CEDARWOOD
705	241	703	1700	8	135	*BENNETT ST TO NEW 10"
706 707	303 291	295 705	1600 1260	8	135 125	*EXTEND HONEY GROVE TO SOUTHLAND
708	705	704	650	8	135	*EXIST ASHLAND LANE *TWILIGHT LANE
709	321	707	730	6	125	*EXIST BET GRANDE AND HILL
710 711	370 369	377 708	1700 1100	8	135	*INGA LANE
712	708	339	700	6 8	125 135	*EXIST CAMINO CABALLO *CAMINO CABALLO
713	710	712	6650	10	135	*FRONTAGE RD SO OF SUMMIT STATION
714 715	712 71 1	375 713	3000 3500	10	135	*FRONTAGE RD
716	713	712	1000	8	125 135	*EXIST 8 INCH *CONNECT TO NEW FRONTAGE RD 10 INCH
102	102	702	400	10	125	
717 718	702 702	103 103	1160 1160	10 12	125 125	*
258	102	701	800	8	125	*PARALLEL LINE *
719	701	259	520	8	125	*
720	703	307	1000	10	135	*
317 721	305 704	704 306	390 398	6	125 125	*
365	330	706	990	8	125	*
722	706	347	980	8	125	*
514 723	430 710	710 414	2570 1890	8	125 125	*

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740 741	197 707	200 706	200 1200	10 8	135 135	* EXIST 10" * NEW HILL ST 8"
			LAKE TIE		135	" NEW HILL SI O"
750	606	750	80	8	135	* TIE IN ON WILLOW RD NEAR BEVINGTON WELL
652	652	751	450	8	125	* TIE NEAR HYDRO TANK
751	631	751	150	8	125	
752						* TIE FROM BARBERRY WAY
	636	752	800	8	135	* TIE MISTY RIDGE TO WILLOW RD
753	650	652	250	8	135	* HYDROTANK BYPASS
173	175	750	640	10	125	* WILLOW RD TIE IN
754	750	179	490	10	125	* WILLOW RD TIE IN
176	179	752	3750	10	125	* WILLOW RD/BARBERRY WAY TIE IN
527	752	182	1200	10	125	* 11 11 11 11
755	187	754	1700	10	135	* POMEROY TIE IN
756	754	753	850	10	135	* 11
757	753	190	2750	10	135	* "
758	641	753	60	8	135	* "K" ST. TIE IN
*759	644	754	60	8	135	* "N" ST. TIE IN
NODES						
700	0 36	5	*LEAF AN	D CEDAR	JOOD	
701	0 360	0	*CEDARWO	OD AND B	BRANCH	
702	0 363	3	*CEDARWO	OD AND	TEFFT	
703	0 290	0	*ALONG N	EW 10"	T AMADO S	ST
704	0 320	0	*STORY S	T AT TW	LIGHT	
705	0 320	0	*TWILIGH			
706	0 39		*HILL ST			
707	0 403		*HILL ST			
708	0 36	H 20	*CAMINO			
710	0 40	5.7			AT FRISCO	UAY
711	0 36					
712	0 36					
713	0 37					
800	0 38		*FRONTAG		E TO STAN	NDPIPE TANK
			LAKE TIE			
750	0	322	0	0	0	
751	ŏ	353	ő	ŏ	õ	
752	ŏ	353	õ	0	0	
753	õ	359		27. I		
754	ŏ	376	0	0	0	
		210	U	U	U	
DEMANDS						
700	-3.74					
701	-2.48					
710	-5.63					
712	-20.2	5				
run						
	PLANWTR	.KEP				
endfile	3					

*NIPOMO	CSD SEW	ER MODEL	OF EXIS	STING SYS	TEM - M	AIN ZONE	TO WWTP
*WWTP1. PAGESIZ					_		
DESIGN	CRITERIA						
ANALYSI PEAKING		IA 0.9 ' 0.9	15 0.9 2	1 0.9 999			
	runrit.0						
	0100	0 0					
GEOMETR *1068	349.5	100	500	325.26	0.011	4	
*1066	348.5	1190	400	311	0.011	4	
1005 1006	289.57 290.54	50 290	1006 1007	290.54 291.41	0.011	15 15	
1007	291.41	400	1008	292.81	0.011	15	
1008 1009	292.81 294.03	420 1300	1009 1010	294.03 302.14	0.011 0.011	15 15	
1010	302.14	360	1011	305.1	0.011	15	
1011	305.1	370	1012	313.33	0.011	12	
1012 1013	313.33 315.72	950 1060	1013 1014	315.72 318.64	0.011 0.011	12 12	
1014	318.64	1130	1015	336.22	0.011	10	
1015 1016	336.22 338.61	850 250	1016 1017	338.61 339.09	0.011 0.011	10 10	
1017	339.09	350	1020	339.99	0.011	10	
1020 1021	339.99 340.88	370 340	1021 1022	340.88	0.011	10 10	
1022	341.79	280	1022	342.96	0.011 0.011	8	
1023	342.96	280	1024	344.14	0.011	8	
1024 1025	344.14 351.13	280 280	1025 1026	351.13 357.33	0.011	8 8	
1026	357.33	220	1027	359.83	0.011	8	
1027 1011	359.83 305.1	500 460	1028 1029	368.47 306.16	0.011 0.011	8 12	
1029	306.16	420	1030	307.19	0.011	12	
1030 1031	307.19	1320	1031	309.97	0.011	12	
1031	309.97 314.36	340 300	1032 1033	314.36 315.71	0.011 0.011	8 8	
1031	309.97	25	1035	329.68	0.011	8	
1035 1035	329.68 329.68	130 520	1036 1037	331.34 331.6	0.011 0.011	8 8	
1034	312.86	1040	1038	315.29	0.011	10	
1031 1034	309.97 312.86	784 304	1034 1038	312.86 315.29	0.011 0.011	12 10	
1038	315.29	400	1039	319.12	0.011	8	
1038	315.29	750	1040	320.58	0.011	10	
1040 1041	320.58 324.85	330 252	1041 1042	324.85 327.28	0.011 0.011	10 8	
1041	324.85	585	1045	329.44	0.011	10	
1045 1043	329.44 339.98	309 227	1043 1044	339.98 341.32	0.011 0.011	8 8	
1044	341.32	380	1046	352.06	0.011	8	
1011	305.1	380	1047	306.02	0.011	12	
1047 1047	306.02	110 300	1048 1049	306.35 311.83	0.011 0.011	12 8	
1049	311.83	320	1050	314.99	0.011	8	
1049 1051	311.83 312.98	240 310	1051 1052	312.98 314.8	0.011 0.011	8 8	
1013	316.21	350	1053	331.75	0.011	8	
1053 1054	331.75 333.34	190 600	1054 1055	333.34 334.99	0.011	8 8	
1054	334.99	260	1056	335.51	0.011	8	
1056	335.51	50	513	337.83	0.011	8	
513 1057	337.84 340.16	50 250	1057 1060	340.16 342.55	0.011	8 8	
1060	342.55	50	1061	342.69	0.011	8	
1061 1062	342.69 346.8	280 270	1062 1063	346.8 364	0.011 0.011	8 8	
1063	364	100	1064	366.86	0.011	8	
1063 1061	364 342.69	100 630	1065 1066	364.5 348.5	0.011	8 8	
1066	348.5	50	1067	348.5	0.011	8	
1067	349	50	1068	349.5	0.011	8	
1016 1069	347.08	50 360	1069 1070	347.42 348.89	0.011 0.011	8 8	
1070	348.89	280	1071	351	0.011	8	
1071 1072	351 356.67	400 400	1072 1073	356.67 359.5	0.011 0.011	8 8	
0.2424/00	1.5.5.5.7.6	8000			and de la	ः • • • • • • • • •	

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*1066 348.5 SANITARY LOADIN	530	1058	353.8	0.011	6
1014 1 1015 1 1016 1 1028 1	-	1.431672 4.820112 1.39128 0.991848	2		
1028 0 1028 0 1033 1	0 0	175.0000 110.0000 0.300000)#		FROM BLACK LAKE MH PARK LS FROM BRACKEN LS
1034 1 1035 1 1036 1		0.318648	2		
1037 1 1038 1 1039 1		0.660432 1.588752 1.588752	2		
1041 1 1042 1 1043 1		0.937992	2		
1043 0 1044 1 1045 1	0	315.0000 1.068144 0.911064	3	*LOADING	FROM TEFFT LS
1046 1 1046 0 1047 1	0	0.318648 175.0000 0.74052		*LOADING	FROM N. OAKGLEN LS
1048 1 1049 1 1050 1		0.74052 0.619344 0.991848			
1051 1 1052 1 1053 1		0.870672 0.74052 1.808664			
1054 1 1055 1 1056 1		2.450448 3.550008 0.251328	5		
1057 1 1061 1 1062 1		0.870672	5		
1063 1 1064 1 1065 1 1066 0	0	0.870672 0.251328 1.238688 175.0000	5	*I DAD INC	FROM NIPOMO PALMS LS
*1066 0 1068 0 1069 1	o o	310.000 190.0000 1.39128	00#	*LOADING	FROM CSA 1 FROM LA MIRADA LS
1070 1 1071 1 1072 1		1.39128 1.39128 1.39128			
1073 0 1057 1 1061 1	0	111.0000 0.870672 0.498168)#	*LOAD ING	FROM GARDENIA LS
1062 1 1063 1 1064 1		0.870672			
1065 1 1069 1 1070 1		1.238688 1.39128 1.39128	3		
1071 1 1072 1 ENDFILE		1.39128 1.377816			

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NUMPOR CO SPUER MORL OF EXISTING TYPER - TEFT ST LE ANGA 202 307.72 203 320.85 0.011 8 PERTURAL - MARCH LE AL												9
101 201.7 2	******			ICTING OVEREN								
101 201.7 2	*NIPOM	D CSD SEWER MC	JDEL OF EX	ISTING SYSTEM	TEFFT	ST LS AREA	-					승규, 위험 영상 전 전 전 전 전 전 전 전 전 전 전 전 전 전 전 전 전 전
101 201.7 2	PACEST	7E 84										
101 201.7 2	DESIGN	CRITERIA O 90	15 0.90	21 0 90 999								
101 201.7 2	ANALYS	IS CRITERIA O.	90 15 0.9	0 21 0.90 999			2				320.41 0	.011 8
101 201.7 2	PEAKIN	G 3.0 0.9					2					
101 201.7 2	OUTPUT	TEFFT3.OUT									343 45 0	
101 201.7 2	UNITS I	0010000					2					
101 201.7 2	GEOMET	RY					2				306.55 0	
101 201.7 2	100	293.7 300	101	300.58 0.0	11 8		2	220			309.67 0	
101 201.7 2	555	291.41 100	100	293.7 0.0	11 8	*TO TEFFT LS	2	221			314.72 0	
101 300.58 450 102 303.6 0.011 8 223 321.64 0.011 224 323.74 0.011 8 104 305.76 250 105 307.87 250 105 307.87 250 106 307.87 0.011 8 223 333.46 0.011 8 105 306.78 250 105 307.87 200 106 307.87 200 106 307.87 200 106 307.87 200 106 307.87 200 106 307.87 200 108 317.57 200 108 317.57 200 108 317.75 0.011 8 223 322.07 0.011 8 232 321.02 200 118 317.54 200 153 319.54 0.011 8 235 334.49 0.011 8 235 334.49 0.011 8 235 334.49 0.011 8 235 334.49 0.011 8 236 334.49 0.011 8 235 335.16 0.011 8	100	293.7 60	156	294.02 0.0	11 8		4			223	321.86 0	
120 333.5. 433.5. 433.5. 433.5. 433.5. 433.5. 440.0111 8 225 333.4.4 0.0111 8 105 337.87 240 106 306.96 0.0111 8 223 333.4.4 0.0111 8 106 306.96 470 107 311.92 0.0111 8 223 332.4.4 20.011 8 107 311.92 200 118 312.3.2 0.0111 8 230 321.02 430 232 322.0 0.011 8 108 311.75 270 151 315.46 0.0111 8 233 324.4 400 123 323.47 6 0.011 8 233 324.4 400 123 323.47 6 0.011 8 233 324.4 400 123 323.47 6 0.011 8 234 323.44 400 123 333.44 0.011 8 234 323.54 6 0.011 8 234 335.46 0.011 8 135 333.44<										224	323.79 0	
133 305.26 300.25 400 226 336.46 0.011 8 135 307.77 240 106 307.77 0.011 8 223 332.45 300 227 334.49 0.011 8 106 306.98 470 107 311.19 200 118 312.22 0.011 8 233 321.22 500 118 314.75 0.011 8 233 323.25 60 0.011 8 233 323.45 400 233 322.67 0.011 8 233 323.45 400 233 323.65 0.011 8 233 323.45 400 123 324.56 0.011 8 233 323.46 400 123 334.76 0.011 8 233 323.46 400 133 320.35 331.45 331.45 331.45 331.45 331.45 331.45 331.46 0.011 8 236 333.44 333.46 0.011 8 236 333.45 331.46 0.011 8 100.11 8 240												
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$ \begin{array}{cccccccccccccccccccccccccccccccccccc$				307.87 0.0	11 8						343.49 0	
$ 107 311.19 220 118 312.22 0.011 8 230 321.02 500 222 322.97 6.011 8 \\ 316.73 220 150 317.76 0.011 8 232 332.85 400 233 323.85 400 233 323.85 400 233 324.85 400 234 325.85 1011 8 236 335.85 1071 8 236 335.85 1071 8 236 335.85 1071 8 236 335.85 1071 241 379.43 1071 8 240 335.45 1071 8 240 335.45 1071 8 240 335.45 1071 8 240 335.45 1071 8 240 335.45 1071 8 240 335.45 1071 8 240 335.45 1071 8 240 335.45 1071 8 240 335.45 1071 8 240 335.45 1071 8 240 335.45 1071 8 240 336.95 400 118 101 1 0.228883 101 1 0.228884 101 1 0.228884 101 1 0.228884 101 1 0.228884 101 1 0.228884 101 1 0.228884 101 1 0.228884 101 1 0.228884 101 1 0.228884 101 1 0.228884 101 1 0.28884 $												
$ 108 314.73 270 150 317.86 0.011 8 \\ 316.75 430 151 319.54 0.011 8 \\ 151 317.54 430 152 330 0.011 8 \\ 151 317.54 430 152 330 0.011 8 \\ 151 317.54 430 152 330 0.011 8 \\ 153 317.54 430 152 330 0.011 8 \\ 154 317.54 430 152 330 0.011 8 \\ 154 325.52 430 155 335.36 0.011 8 \\ 155 325.54 400 190 370.4 0.011 8 \\ 156 325.54 400 190 370.4 0.011 8 \\ 126 305.4 400 120 335.46 0.011 8 \\ 109 309.41 160 100 310.61 0.011 8 \\ 240 335.55 507 242 335.4 0.011 8 \\ 111 321.00 280 112 322.37 0.011 8 \\ 240 335.55 563 370 242 335.45 0.011 8 \\ 111 321.00 280 112 322.37 0.011 8 \\ 113 321.00 280 112 322.37 0.011 8 \\ 114 322.66 320 115 322.11 0.011 8 \\ 115 325.66 370 242 335.5 5 0.011 8 \\ 113 321.00 280 112 322.37 0.011 8 \\ 114 322.66 320 115 322.11 0.011 8 \\ 116 122 0 2368.9 430 \\ 117 331.89 300 120 336.48 0.011 8 \\ 102 1 1 0.6873.4 \\ 115 325.66 320 116 326.44 0.011 8 \\ 106 1 0 0.5873.4 \\ 115 325.66 370 122 336.48 0.011 8 \\ 106 1 0 0.5873.4 \\ 117 331.89 300 120 336.48 0.011 8 \\ 106 1 0 0.5873.4 \\ 117 336.48 230 121 336.48 0.011 8 \\ 106 1 0 0.4973.4 \\ 123 336.42 230 121 336.48 0.011 8 \\ 110 1 0 0.4973.4 \\ 123 336.42 230 121 336.48 0.011 8 \\ 110 1 0 0.4973.4 \\ 123 336.42 230 121 336.48 0.011 8 \\ 110 1 0 0.4973.4 \\ 123 336.42 230 123 336.48 0.011 8 \\ 110 1 0 0.4973.4 \\ 123 336.42 230 123 336.48 0.011 8 \\ 110 1 0 0.4973.4 \\ 123 336.42 230 123 336.42 0.011 8 \\ 110 1 0 0.4973.4 \\ 123 336.42 300 123 336.42 0.011 8 \\ 110 1 0 0.4973.4 \\ 123 336.42 300 123 336.44 0 0.4971.68 \\ 131 1 0 0.4971.68 \\ 131 1 0 0.4971.68 \\ 131 0 0.4971.68 \\ 131 0 0.4$												
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227	1	0.74052
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232	i	1.238688
233	i	0.870672
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235	1	1.122
236		0.74052
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241	1	1.490016
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401	311.10	50	402	312.49	0.011	8				
402	312.49		403	321.7	0.011	8				
403 403	321.7 321.7	200 220	404 405	325.8 328.01	0.011	8 8				
405	328.01	90	406	330.36	0.011	8				
406	330.36	110	407	331.32	0.011	8				
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409	329.05	130	410	329.55	0.011	8				
410	329.55	450	411	334.1	0.011	6				
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400	311.00	140	430	311.25	0.011	8				
430	311.25	30	431	314	0.011	6				
431 432	314 332	200 220	432 433	332 339.7	0.011	6				
431	314	430	433	322.46	0.011	6				
434	322.46	200	435	326.4	0.011	6				
435 435	326.4 326.4	260 260	436 437	342 340.35	0.011 0.011	6 6				
437	340.35	370	438	340.52	0.011	6				
402		370	414	313.55	0.011	8				
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415	314.09	70	417	314.48	0.011	8 8				
417	314.78	380	420	315.95	0.011	8				
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422	317.52	220	422	322.7	0.011	8 8				
423	322.7	180	424	331	0.011	8				
423 422	322.7 317.52	220 200	425 426	331 318.53	0.011	8				
426	318.53	140	420	319.39	0.011	8				
422	317.52	180	428	318.7	0.011	8				
428 SANIT/	318.7 ARY LOADIN	120	429	330	0.011	8				
402	1	G	0.6193	44						
403	1		0.4981	68				435	1	0.74052
404 405	1		0.7405					436	i	1,122
405	i		0.8482					437	1	0.870672
407	1		0.8482	32				438 ENDFILE	1	0.368016
408	1		0.8482					CHUITLE		
409	1		0.7405							
410	1			000# * CSA	-1					
412 413	1		0.4577							
414	1		0.4577							
414	1		0.7405	2 *PREVIO	U	SLY W	AS AT NODE 439			
415 416	1		0.8482							
417	i		0.8482							
420	1		0.8482	32						
421 422	1		0.8482							
423	i		0.8482							
424	1		0.4577	76						
425 426	1		0.8482							
427	1		1.0412							
429	1		0.4577	76						
430 432	1		0.6193							
433	1		0.9918	48						
434	1		1.6111	92						

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*NIPOMO CSD SEWER MODEL OF EXISTING SYSTEM - BRACKEN LS AREA *BRACKEN.DTA PAGESIZE 84 DESIGN CRITERIA 0.9 15 0.9 21 0.9 999 ANALYSIS CRITERIA 0.9 15 0.9 21 0.9 999 PEAKING 3.0 1 OUTPUT BRACKEN3.OUT UNITS 0 0 1 0 0 0 0 GEOMETRY 331 336.51 0.011 8 330 333.8 150 336.51 60 337.6 0.011 8 331 332 339.46 0.011 332 337.6 230 333 8 339.24 0.011 334 8 332 337.6 80 SANITARY LOADING 0.368016 331 1 0.368016 331 1 332 0.251328 1 0.74052 333 1 334 0.251328 1 ENDFILE

*NIPOMO CSD SEWER MODEL OF EXISTING SYSTEM - NORTH OAK GLEN LS AREA *NOAKGLEN.DTA PAGESIZE 84 DESIGN CRITERIA 0.9 15 0.9 21 0.9 999 ANALYSIS CRITERIA 0.9 15 0.9 21 0.9 999 PEAKING 3.0 1 OUTPUT NOAK3.OUT UNITS 0 0 1 0 0 0 0 GEOMETRY 332.85 140 341.3 0.011 163 164 8 165 163 332.85 230 333.76 0.011 8 326.81 100 332.85 0.011 222 163 8 165 333.76 380 166 335.4 0.011 8 336.95 0.011 335.4 310 167 166 8 336.95 600 167 168 346.48 0.011 8 SANITARY LOADING 0.251328 164 1 164 0.318648 1 165 0.498168 1 166 1 0.498168 2.31132 167 1 168 1 0.991848 ENDFILE

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*NIPOMO *MHPBLA		ER MODEL	OF EXIS	TING SYS	STEM - E	BLACK	LAKE MHP LS AREA
PAGESIZ							
	CRITERIA	0.9.1	5 0.90 2	1 0.90	000		
	S CRITER						
	3.0 0.9						
	MHPBL3.0	TU					
UNITS 0	0100	0 0					
GEOMETR							
300	343.73	60	301	349.01	0.011	8	
999	334.93	100	300	343.73	0.011		*TO BLACK LAKE LS @ MHP
301 302	349.01 350.58	400	302	350.58	0.011	8	
302	351.22	130 300	303 304	351.22	0.011	8 8	
304	352.72	140	305	353.55	0.011 0.011	8	
305	353.55	120	306	354.05	0.011	8	
306	354.05	230	307	356.37	0.011	8	
307	356.37	300	308	378.7	0.011	8	
306	354.05	190	309	355.22	0.011	8	
309	355.22	100	310	362	0.011	8	
300	343.73	90	250	345.09	0.011	8	
250 *250	345.09 345.09	150 342	311 251	350.46 348	0.011	8	the can Leapthe
311	350.46	10	312	351.08	0.011 0.011	8 8	*NO SAN. LOADING
312	351.08	280	313	367.02	0.011	6	
313	367.02	280	314	369.17	0.011	6	
*315	357.02		314	369.17	0.011	6	*REDUNDANT
315	357.02	120	316	357.26	0.011	6	
312	351.08	260	317	352.18	0.011	6	
317	352.18	100	329	354.98	0.011	8	
329	354.98	330	327	356.22	0.011	8	
327 327	356.22	150 470	315 328	357.02	0.011	6	
317	352.18	280	320	367.22 361.13	0.011	6	
320	361.13	280	321	375.33	0.011	6	
320	361.13	260	322	377.75	0.011	6	
322	377.75	260	323	390.93	0.011	6	
322	377.75	280	324	379.05	0.011	6	
324	379.05	380	325	398.32	0.011	6	
325	398.32	200	326	403	0.011	6	
303	Y LOADIN	0.61934	4				
304	i	0.74052					
305	i	0.36801					
306	1	3.04434					
307	1	0.87067	2				
308	1	0.74052					
309	1	0.49816					
310	1	0.49816					
311 313	i	0.61934					
314	i	0.99184					
315	i	0.87067					
316	1	0.25132	8				
317	1	0.87067					
320	1	0.87067					
321	1	0.87067					
322 323	1	0.87067					
324	1	1.23868					
325	1	1.23868					
326	i	0.61934					
327	1	0.87067	2				
328	1	1.23868	8				
ENDET1 F							

328 1 ENDFILE

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*NIPOMO	CSD SEW	ER MODEL	OF EXIS	TING SYS	TEM - LA	MIRADA LS	AREA
*LAMIRA	DA.DTA				_		
PAGESIZ							
				0.95			
			15 0.90	21 0.95	999		
	3.0 0.9						
	LAMIRAD3						
	0100	0 0					
GEOMETR			1440 C 101 C 101				
500	325.26	440	501	327.13	0.011	8	
501	327.13	100	502	332	0.011	6	
501	327.13	250	503	329.1	0.011	8	
503	329.1	200	504	334.5	0.011	8	
503	329.1	470	505	348.7	0.011	8	
505	348.7	170	506	349.8	0.011	8	
500	325.26	280	507	336	0.011	8	
507	336	290	508	350.86	0.011	8	
507	336	230	509	338.62		8	
509	338.62	120	510	339.99		8	
555	326.70	100	500	327.13	0.011	8 *INTO	LA MIRADA LS
	Y LOADIN	G					
500	1		0.77				
501	1		1.122		OUSLY AT	NODE 500	
501	1		2.13884				
502	1		0.25132	8			
503	1		1.61119	2			
504	1		0.87067	2			
505	1		0.99184	8			
506	1		0.61934	4			
507	1		1.122				
508	1		0.49816	8			
509	1		0.99184	8			
510	1		0.25132	28			
*511	1		1.2386	88	* TO W	TP DIRECT	LY
*512	1		1.3688	34	*	11	
*513	1 1		0.2513	28	*	14	
*514	1		0.8706	572	*	14	
*515	1		0.7405	2	*		
ENDELLE							

ENDFILE

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*NIPOMO CSD SEWER MODEL OF EXISTING SYSTEM-BLACK LAKE DEVELOPMENT *WOODGRN.DTA PAGESIZE 84 DESIGN CRITERIA 0.5 15 ANALYSIS CRITERIA 0.5 15 PEAKING 2.0 1 OUTPUT BLACKLKE.OUT GEOMETRY .011 .011 .011 .011 .011 .011 .011 .011 .011 .011 .011 .011 .011 .011 .011 .011 SANITARY LOADING ENDFILE

*NIPOMO CSD SEWER MODEL OF EXISTING SYSTEM - GARDENIA LS AREA *GARDENIA.DTA PAGESIZE 84 DESIGN CRITERIA 0.9 15 0.90 21 0.90 999 ANALYSIS CRITERIA 0.9 15 0.90 21 0.90 999 PEAKING 3.0 0.9 OUTPUT GARDEN3.OUT UNITS 0 0 1 0 0 0 0 GEOMETRY 338.6 0.11 361.5 361.5 375.52 0.11 361.5 362.76 0.11 362.76 270 363.44 0.11 362.76 280 363.48 0.11 SANITARY LOADING 0.498168 0.619344 0.74052 0.498168 0.2 0.251328 ENDFILE

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*NIPOMO *FWWTP1.		ER MODEL	OF EXIST	TING SYS	TEM,	FUTURE	FLOWS 9/8/	95	
PAGESIZ						MAIN	ZONE	07	9 JUW
	Contraction of the second second	0.90 15	0.90 21	0.90 99	9				
		IA 0.90	15 0.90 2	21 0.90	999				
PEAKING		0.9							
	0 1 0 0								
GEOMETRY		00							
*1068	349.5	100	500	325.26	0.01	1 4			
*1066	348.5	1190	400	311	0.01				
1005	289.57	50	1006	290.54	0.01				
1006 1007	290.54	290	1007	291.41 292.81	0.01				
1008	292.81	420	1009	294.03	0.01				
1009	294.03	1300	1010	302.14	0.01				
1010	302.14	360	1011	305.1	0.01				
1011	305.1	370	1012	313.33	0.01				
1012 1013	313.33 315.72	950 1060	1013 1014	315.72 318.64	0.01				
1014	318.64	1130	1015	336.22	0.01				
1015	336.22	850	1016	338.61	0.01				
1016	338.61	250	1017	339.09	0.01				
1017 1020	339.09	350 370	1020 1021	339.99 340.88	0.01				
1021	340.88	340	1022	341.79	0.01				
1022	341.79	280	1023	342.96	0.01				
1023	342.96	280	1024	344.14	0.01	1 8			
1024	344.14	280	1025	351.13	0.01				
1025 1026	351.13	280 220	1026 1027	357.33 359.83	0.01	12 U - 13 Er			
1027	359.83	500	1028	368.47	0.01				
1011	305.1	460	1029	306.16	0.01				
1029	306.16	420	1030	307.19	0.01	12			
1030	307.19	1320	1031	309.97	0.01				
1031 1032	309.97 314.36	340 300	1032 1033	314.36 315.71	0.01				
1031	309.97	25	1035	329.68	0.01				
1035	329.68	130	1036	331.34	0.01				
1035	329.68	520	1037	331.6	0.01				
1034 1031	312.86 309.97	1040 784	1038 1034	315.29 312.86	0.01				
1034	312.86	304	1034	315.29	0.01	4 A A A A A A A A A A A A A A A A A A A			
1038	315.29	400	1039	319.12	0.01				
1038	315.29	750	1040	320.58	0.01				
1040	320.58	330	1041	324.85	0.01				
1041 1041	324.85 324.85	252 585	1042 1045	327.28	0.01				
1045	329.44	309	1043	339.98	0.01				
1043	339.98	227	1044	341.32	0.01	1 8			
1044	341.32	380	1046	352.06	0.01				
1011 1047	305.1 306.02	380 110	1047 1048	306.02	0.01	10 10 10 10			
1047	306.02	300	1048	311.83	0.01				
1049	311.83	320	1050	314.99	0.01				
1049	311.83	240	1051	312.98	0.01				
1051 1013	312.98	310	1052 1053	314.8	0.01				
1053	316.21 331.75	350 190	1055	331.75 333.34	0.01				
1054	333.34	600	1055	334.99	0.01				
1054	334.99	260	1056	335.51	0.01	1 8			
1056	335.51	50	513	337.83	0.01				
513 1057	337.84 340.16	50 250	1057 1060	340.16 342.55	0.01				
1060	342.55	50	1061	342.69	0.01				
1061	342.69	280	1062	346.8	0.01				
1062	346.8	270	1063	364	0.01				
1063 1063	364 364	100	1064 1065	366.86	0.01				
1065	342.69	630	1066	364.5	0.01				
1066	348.5	50	1067	349	0.01				
1067	349	50	1068	349.5	0.01	1 8			
1016	347.08	50	1069	347.42	0.01				
1069 1070	347.42 348.89	360 280	1070 1071	348.89 351	0.01				
1071	351	400	1072	356.67	0.01				
1072	356.67	400	1073	359.5	0.01	1 8			
					Conv	of docum	ent found at	14/14/14	NoNow/Mir

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1080 325.49 2200 358.69 0.011 8 *GRANDE AVE 1081 1014 318.64 800 1080 325.49 0.011 8 *1066 348.5 530 1058 353.8 0.011 6 * NIPOMO PALMS LS ELIMINATION PIPELINE *1100 310.75 150 400 311.0 .011 8 *1101 1100 310.04 470 .011 310.75 8 *1102 309.2 560 1101 310.04 .011 8 1103 308.51 360 1102 309.20 .011 8 1104 307.95 350 308.51 1103 .011 8 1105 307.10 500 1104 307.95 .011 8 1048 306.35 500 1105 307.10 .011 8 SANITARY LOADING 1009 36.96 *Added-new: Southland Street 1 1011 14.81 *Added-new: Story Street 1 1012 7.84 *Added-new 1 10.74 1013 *Added-new: Division Street 1 1014 49.411672 *Grand Ave 1 1015 53.380112 1 1016 5.07128 1 1017 1 3.68 *Added-new 1020 3.68 *Added-new 1 1021 4.71 *Added-new 1022 *Added-new 31.93 1 1023 1.55 *Added-new 1 12.50 *Added-new:Tie in Pradera Septic 1024 1 *Added-new 1025 1 1.55 1026 *Added-new 1 0.0 1028 0.991848 1 1028 0 0 175.0000# *LOADING FROM BLACK LAKE MH PARK LS *LOADING FROM BRACKEN LS 1028 0 0 110.0000# 1030 1 10.31 *Added-new 1031 0.41 *Added-new 1 1032 *Added-new 1 0.21 1033 0.710000 1 1034 11.828648 1 1035 1 1.070432 1036 0.300000 1 1036 100.000000# *PROPOSED AMADO ST LS 1 1037 0.660432 1 1038 1.588752 1 1039 1.998752 1 1040 1 6.22 *Added-new 1041 6.067992 1 1042 0.708168 1 1043 1 4.851064 1043 0 0 600.0000# *LOADING FROM UPGRADED TEFFT LS 1044 1 1.068144 1045 1 0.911064 1046 0.318648 1 1046 0 0 175.0000# *LOADING FROM N. OAKGLEN LS 0.74052 1047 1 1048 0.74052 1 1048 1 5.0 *LOADING FROM MONTECITO VERDE I 1049 1 0.619344 1050 0.991848 1 1051 1 0.870672 1052 0.74052 1 1053 1.808664 1 1054 3.400448 1 1055 3.550008 1 1056 1 1.061328 1057 0.870672 1 1061 1 0.498168 1062 1 0.870672 1063 1 0.870672 1064 1 0.251328 1065 1 1.238688 *1066 0 0 175.0000# *LOADING FROM NIPOMO PALMS LS *1066 0 0 310.0000# *LOADING FROM CSA 1 1066 0 *PROPOSED MERCURY COURT LS 0 190.0000# 1068 0 0 190.0000# *LOADING FROM LA MIRADA LS 1069 1 5.07128 1070 1 1.39128 1071 1.39128 1 1072 1 1.377816 1073 1 1.72 111.0000# 0 *LOADING FROM GARDENIA LS 1073 0 1081 12.94 1 *Added-new Copy of document found at www.NoNewWipTax.com

1057	1	0.870672	
1061	1	0.498168	
1062	1	0.870672	
1063	1	0.870672	
1064	1	0.251328	
1065	1	1.238688	
1069	1	1.39128	
1070	1	1.39128	
1071	1	1.39128	
1072	1	1.377816	
1102	1	5.2	*LOAD
1104	1	11.13	*LOAD
ENDFIL	E		

*LOADING FROM MONTECITO VERDE II *LOADING FROM EAST OF CRYSTAL WAY BOTH SIDES OF STORY ST. ÷

PAGESIZE 84 DESIGN CRITERIA 0.90 15 0.90 21 0.90 999 PANALYSIS CRITERIA 0.90 15 0.90 21 0.90 999 PEAKING 3 0.9 COUPUT FTEFT.CUT UNITS 0 0 1 0 0 0 0 GEOMETRY 100 223.7 60 156 294.02 0.011 8 101 300.58 450 102 333.6 0.011 8 102 303.6 400 103 305.26 0.011 8 103 305.26 360 104 336.78 0.011 8 104 306.78 250 105 307.87 0.011 8 105 307.87 240 106 338.48 0.011 8 106 306.98 470 107 311.99 0.011 8 108 314.73 420 108 314.73 0.011 8 108 314.73 430 151 319.54 0.011 8 108 314.73 430 152 330 0.011 8 151 319.54 400 152 330 0.011 8 153 320.35 6 400 109 320.45 0.011 8 154 325.62 460 152 330 0.011 8 155 320.35 260 104 336.78 0.011 8 151 319.54 400 152 330 0.011 8 154 325.62 460 152 330 0.011 8 154 325.62 460 152 335.08 0.011 8 154 325.62 460 153 322.03 0.011 8 154 325.62 400 154 325.62 0.011 8 154 325.62 400 195 335.08 0.011 8 154 325.62 400 195 335.08 0.011 8 154 325.62 400 195 335.08 0.011 8 154 325.62 400 116 310.81 0.011 8 109 309.41 160 110 310.81 0.011 8 111 321.09 250 112 322.39 0.011 8 111 321.09 250 113 332.19 0.011 8 111 321.09 250 113 332.10 0.011 8 111 321.09 175 114 322.96 0.011 8 111 321.09 175 114 322.96 0.011 8 113 31.99 300 120 338.48 0.011 8 114 322.96 520 115 335.06 0.011 8 115 325.06 375 117 331.99 0.011 8 120 338.48 250 121 339.97 0.011 8 121 339.97 175 122 344.11 0.011 8 122 344.11 410 123 342.47 0.011 8 123 309.24 140 125 339.48 0.011 8 124 316.44 400 125 319.48 0.011 8 125 319.78 370 150 338.48 0.011 8 126 327.42 400 141 312.89 0.011 8 127 332.43 400 126 327.42 0.011 8 131 322.09 230 132 334.42 0.011 8 132 334.42 030 142 336.24 0.011 8 133 34.41 1260 130 340.42 360.11 8 134 345.18 330 129 332.43 30.118 8 135 34.44 100 126 337.42 0.011 8 136 357.1 30.118 8 137 324.54 400 126 337.42 0.011 8 136 357.1 30.118 8 137 324.54 400 126 337.42 0.011 8 136 357.1 30.118 8 137 324.54 400 126 337.42 0.011 8 136 357.1 30.118 8 137 334.41 260 134 3311.76 0.011 8 136 357.1 30.011 8 137 334.42 104 147 315.62 0.011 8 136 357.1 30.011 8 136 357.1 30.011 8 137 334.42 104 147 315.62 0.011 8 138 34.45.18 330 143 311.76 0.011 8 14			ER MODEL	OF EXIS	STING SYS		FUTURE FLOWS TEFFT ST LS AREA
ANALYSIS CRITERIA 0.90 15 0.90 21 0.90 999 PEAKING 3.0 0.9 CUTPUT FTEFT.CUT UNITS 0 0 1 0 0 0 0 ECOMETRY 100 293.7 60 101 300.58 0.011 8 101 300.58 450 102 303.6 0.011 8 102 303.6 400 103 305.26 0.011 8 103 305.26 360 104 306.78 0.011 8 104 306.78 250 105 307.87 0.011 8 105 307.87 240 106 308.98 0.011 8 106 308.98 470 107 311.99 0.011 8 107 311.9 220 118 312.32 0.011 8 118 312.42 260 108 314.73 0.011 8 108 314.73 430 151 319.54 0.011 8 108 314.73 270 150 317.86 0.011 8 151 319.54 400 152 330 0.011 8 153 320.52 640 155 335.08 0.011 8 154 325.62 460 155 335.08 0.011 8 154 325.62 460 152 330 0.011 8 155 320.56 400 192 320.35 0.011 8 154 325.62 400 152 330 0.011 8 155 320.56 400 192 39.41 0.011 8 154 325.62 400 193 39.41 0.011 8 154 310.54 400 152 330 0.011 8 154 310.54 400 152 332.03 0.011 8 154 310.54 400 152 335.08 0.011 8 154 310.54 400 152 335.08 0.011 8 154 310.54 400 193 39.41 0.011 8 154 310.24 200 153 320.35 0.011 8 154 310.24 1140 110 310.81 0.011 8 154 312.90 175 114 322.90 0.011 8 151 319.54 200 175 133 320.35 0.011 8 154 325.06 260 116 326.44 0.011 8 151 312.90 215 335.08 0.011 8 151 312.90 215 335.06 0.011 8 151 312.90 175 114 322.96 0.011 8 151 312.90 175 114 322.96 0.011 8 151 325.06 260 116 326.44 0.011 8 151 325.06 260 116 326.44 0.011 8 151 325.06 375 117 331.99 0.011 8 151 325.06 375 117 331.99 0.011 8 152 330.52 622 115 332.08 0.011 8 153 325.06 375 117 331.99 0.011 8 152 330.52 620 162 332.287 0.011 8 153 325.06 375 117 331.99 0.011 8 153 325.06 320 120 338.48 0.011 8 153 325.06 327 117 332.243 0.011 8 154 365.18 330 126 337.72 0.011 8 152 310.84 250 142 316.24 0.011 8 152 310.84 250 142 316.24 0.011 8 154 331.76 400 126 327.42 0.011 8 154 331.76 400 142 335.36 0.011 8 155 324.24 300 128 338.23 0.011 8 154 331.76 400 142 335.34 0.011 8 157 305.64 300 128 333.34.41 0.0	PAGESIZ	E 84					TEFT St CS
PEAKING 3.0 0.9 CUTPUT FFFFT.CUT UNITS 0 0 1 0 0 0 0 2004ETRY 555 291.41 100 100 293.7 0.011 8 101 300.58 450 102 303.6 0.011 8 102 303.6 400 103 305.26 0.011 8 103 305.26 360 104 306.78 0.011 8 104 306.78 250 105 307.87 0.011 8 105 307.87 240 106 308.98 0.011 8 105 307.87 240 106 308.98 0.011 8 105 307.87 240 107 311.19 0.011 8 106 306.98 470 107 311.19 0.011 8 107 311.19 220 118 312.32 0.011 8 108 314.73 270 150 317.86 0.011 8 108 314.73 420 105 337.86 0.011 8 108 314.73 420 105 337.86 0.011 8 108 314.73 420 152 330 0.011 8 108 314.73 420 153 320.35 0.011 8 109 30.4 160 153 320.35 0.011 8 151 319.54 400 152 330 0.011 8 153 320.35 260 154 325.62 0.011 8 154 325.26 460 109 309.41 0.011 8 109 30.4 160 100 310.81 0.011 8 100 310.81 310 111 321.09 0.011 8 111 321.09 250 112 322.39 0.011 8 111 321.09 250 112 322.39 0.011 8 111 321.09 250 112 322.39 0.011 8 111 321.09 250 112 322.49 0.011 8 112 325.66 326 116 326.44 0.011 8 113 325.66 326 117 331.99 3.011 8 114 322.96 320 112 332.41 0.011 8 115 325.66 375 117 331.99 3.011 8 121 339.97 175 122 344.11 0.011 8 122 344.11 400 123 342.87 0.011 8 123 305.26 430 120 338.48 0.011 8 134 340.42 316.44 0.011 8 144 312.49 240 142 316.24 0.011 8 145 310.52 430 121 339.47 0.011 8 146 303.62 430 132 334.48 0.011 8 147 315.62 370 129 332.43 0.011 8 148 341.4 36.44 0.011 8 149 310.52 430 142 315.20 0.011 8 141 312.97 240 142 336.24 0.011 8 144 311.76 140 142 332.43 0.011 8 145 311.76 140 142 333.22 0.011 8 146 311.47 180 162 335.48 0.011 8 147 315.62 370 159 332.43 0.011 8 146 311.47 180 162 335.44 0.011 8 147 315.62 370 157 335.46 40 0.011 8 146 311.47 180 161 311.47 0.011 8 147 315.62 370 157 335.46 0.011 8 146 311.47 180 162 335.40 0.011 8 147 315.62 370 157 335.46 0.011 8 146 311.47 18							
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132334.82350133344.1 0.011 8133344.1260134345.18 0.011 8134345.18330135346.64 0.011 8135346.64250136357.1 0.011 8136357.1330137367.96 0.011 8106308.98430143311.76 0.011 8143311.76190144314.93 0.011 8143311.76460145314.33 0.011 8145318.37110146319.36 0.011 8147315.62370148319.95 0.011 8147315.62370148319.95 0.011 8147315.62370148319.95 0.011 8147315.62370146319.21 0.011 8147315.62370157305.66 0.011 8156294.2370157305.66 0.011 8160311.1180161311.67 0.011 8160311.1180161311.67 0.011 8160311.1180162325.4 0.011 8161311.67180162325.4 0.011 8200299.4470201301.31 0.011 8201301.31 </td <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>1 8</td>							1 8
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135 346.64 250 136 357.1 0.011 8 136 357.1 330 137 367.96 0.011 8 106 308.98 430 143 311.76 0.011 8 143 311.76 190 144 314.93 0.011 8 143 311.76 460 145 314.33 0.011 8 143 311.76 460 145 314.33 0.011 8 145 318.37 110 146 319.36 0.011 8 107 311.19 420 147 315.62 0.011 8 147 315.62 370 148 319.95 0.011 8 147 315.62 370 148 319.95 0.011 8 147 315.62 370 148 319.95 0.011 8 160 293.7 70 156 294.02 0.011 8 156 294.2 370 157 305.66 0.011 8 160 311.11 80 161 311.67 0.011 8 161 311.67 180 162 325.4 0.011 8 200 299.4 470 201 301.31 0.011 8 201 301.31 190 202 302.5 0.011 8 202 302.5 220 203 309.42 0.011 8 204 305.2 230				134			1 8
106 308.98 430 143 311.76 0.011 8 143 311.76 190 144 314.93 0.011 8 143 311.76 460 145 314.33 0.011 8 145 318.37 110 146 319.36 0.011 8 147 315.62 370 148 319.95 0.011 8 147 315.62 370 148 319.95 0.011 8 147 315.62 370 148 319.95 0.011 8 147 315.62 370 148 319.21 0.011 8 100 293.7 70 156 294.02 0.011 8 156 294.2 370 157 305.66 0.011 8 156 294.2 370 157 305.66 0.011 8 160 311.11 80 161 311.67 0.011 8 160 311.11 80 161 311.67 0.011 8 160 311.11 80 162 325.4 0.011 8 200 299.4 470 201 301.31 0.011 8 201 301.31 190 202 302.5 0.011 8 202 302.5 220 203 309.42 0.011 8 204 305.2 230 205 319.92 0.011 8 204 </td <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>1 8</td>							1 8
143 311.76 190 144 314.93 0.011 8 143 311.76 460 145 314.33 0.011 8 145 318.37 110 146 319.36 0.011 8 145 318.37 110 146 319.36 0.011 8 107 311.19 420 147 315.62 0.011 8 147 315.62 370 148 319.95 0.011 8 147 315.62 340 149 319.21 0.011 8 100 293.7 70 156 294.02 0.011 8 156 294.2 370 157 305.66 0.011 8 157 305.66 180 160 311.11 0.011 8 160 311.11 80 161 311.67 0.011 8 160 311.11 80 161 311.67 0.011 8 100 293.7 330 200 299.4 0.011 8 100 293.7 330 200 299.4 0.011 8 201 301.31 190 202 302.5 0.011 8 202 302.5 220 203 309.42 0.011 8 204 305.2 230 205 319.92 0.011 8 204 305.2 270 206 306.59 0.011 8	136	357.1	330	137	367.96	0.01	1 8
143 311.76 460 145 314.33 0.011 8 145 318.37 110 146 319.36 0.011 8 107 311.19 420 147 315.62 0.011 8 147 315.62 370 148 319.95 0.011 8 147 315.62 370 148 319.95 0.011 8 147 315.62 340 149 319.21 0.011 8 100 293.7 70 156 294.02 0.011 8 156 294.2 370 157 305.66 0.011 8 157 305.66 180 160 311.11 0.011 8 160 311.11 80 161 311.67 0.011 8 160 311.11 80 161 311.67 0.011 8 100 293.7 330 200 299.4 0.011 8 100 293.7 330 200 299.4 0.011 8 201 301.31 190 202 302.5 0.011 8 202 302.5 220 203 309.42 0.011 8 204 305.2 2302 309.42 0.011 8 204 305.2 230 205 319.92 0.011 8					311.76		1 8
145 318.37 110 146 319.36 0.011 8 107 311.19 420 147 315.62 0.011 8 147 315.62 370 148 319.95 0.011 8 147 315.62 340 149 319.21 0.011 8 147 315.62 340 149 319.21 0.011 8 100 293.7 70 156 294.02 0.011 8 156 294.2 370 157 305.66 0.011 8 157 305.66 180 160 311.11 0.011 8 160 311.11 80 161 311.67 0.011 8 161 311.67 180 162 325.4 0.011 8 100 293.7 330 200 299.4 0.011 8 200 299.4 470 201 301.31 0.011 8 201 301.31 190 202 302.5 0.011 8 202 302.5 220 203 309.42 0.011 8 204 305.2 230 205 319.92 0.011 8 204 305.2 270 206 306.59 0.011 8							1 8
147 315.62 370 148 319.95 0.011 8 147 315.62 340 149 319.21 0.011 8 100 293.7 70 156 294.02 0.011 8 156 294.2 370 157 305.66 0.011 8 156 294.2 370 157 305.66 0.011 8 157 305.66 180 160 311.11 0.011 8 160 311.11 80 161 311.67 0.011 8 161 311.67 180 162 325.4 0.011 8 100 293.7 330 200 299.4 0.011 8 200 299.4 470 201 301.31 0.011 8 201 301.31 190 202 302.5 0.011 8 202 302.5 220 203 309.42 0.011 8 202 302.5 430 204 305.2 0.011 8 204 305.2 230 205 319.92 0.011 8 204 305.2 270 206 306.59 0.011 8	145	318.37		146	319.36	0.01	1 8
147 315.62 340 149 319.21 0.011 8 100 293.7 70 156 294.02 0.011 8 156 294.2 370 157 305.66 0.011 8 157 305.66 180 160 311.11 0.011 8 160 311.11 80 161 311.67 0.011 8 161 311.67 180 162 325.4 0.011 8 100 293.7 330 200 299.4 0.011 8 200 299.4 470 201 301.31 0.011 8 201 301.31 190 202 302.5 0.011 8 202 302.5 220 203 309.42 0.011 8 202 302.5 430 204 305.2 0.011 8 204 305.2 230 205 319.92 0.011 8 204 305.2 270 206 306.59 0.011 8							18
156 294.2 370 157 305.66 0.011 8 157 305.66 180 160 311.11 0.011 8 160 311.11 80 161 311.67 0.011 8 161 311.67 180 162 325.4 0.011 8 161 311.67 180 162 325.4 0.011 8 100 293.7 330 200 299.4 0.011 8 200 299.4 470 201 301.31 0.011 8 201 301.31 190 202 302.5 0.011 8 202 302.5 220 203 309.42 0.011 8 202 302.5 430 204 305.2 0.011 8 204 305.2 230 205 319.92 0.011 8 204 305.2 270 206 306.59 0.011 8	147	315.62		149	319.21	0.01	1 8
157 305.66 180 160 311.11 0.011 8 160 311.11 80 161 311.67 0.011 8 161 311.67 180 162 325.4 0.011 8 100 293.7 330 200 299.4 0.011 8 200 299.4 470 201 301.31 0.011 8 201 301.31 190 202 302.5 0.011 8 202 302.5 220 203 309.42 0.011 8 202 302.5 220 203 309.42 0.011 8 202 302.5 430 204 305.2 0.011 8 204 305.2 230 205 319.92 0.011 8 204 305.2 270 206 306.59 0.011 8							1 8
160 311.11 80 161 311.67 0.011 8 161 311.67 180 162 325.4 0.011 8 100 293.7 330 200 299.4 0.011 8 200 299.4 470 201 301.31 0.011 8 201 301.31 190 202 302.5 0.011 8 202 302.5 220 203 309.42 0.011 8 202 302.5 430 204 305.2 0.011 8 204 305.2 230 205 319.92 0.011 8 204 305.2 270 206 306.59 0.011 8							1 8
200 299.4 470 201 301.31 0.011 8 201 301.31 190 202 302.5 0.011 8 202 302.5 220 203 309.42 0.011 8 202 302.5 220 203 309.42 0.011 8 202 302.5 430 204 305.2 0.011 8 204 305.2 230 205 319.92 0.011 8 204 305.2 270 206 306.59 0.011 8	160	311.11	80	161	311.67	0.01	1 8
200 299.4 470 201 301.31 0.011 8 201 301.31 190 202 302.5 0.011 8 202 302.5 220 203 309.42 0.011 8 202 302.5 220 203 309.42 0.011 8 202 302.5 430 204 305.2 0.011 8 204 305.2 230 205 319.92 0.011 8 204 305.2 270 206 306.59 0.011 8							1 8
202 302.5 430 204 305.2 0.011 8 204 305.2 230 205 319.92 0.011 8 204 305.2 270 206 306.59 0.011 8	200	299.4	470	201	301.31	0.01	1 8
202 302.5 430 204 305.2 0.011 8 204 305.2 230 205 319.92 0.011 8 204 305.2 270 206 306.59 0.011 8							1 8
204 305.2 230 205 319.92 0.011 8 204 305.2 270 206 306.59 0.011 8							1 8
		305.2	230	205	319.92	0.01	1 8
200 300.37 200 207 307.43 0.011 8	204	305.2	270	206	306.59	0.01	
206 306.59 420 208 317.78 0.011 8							

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208 317.78 250	209 320 0.011	8	148 1	0.870672	*No new flow
204 305.2 430 210 316.63 330	210 316.63 0.011 211 319 0.011	8	149 1 150 1	1.201328	No new riter
210 316.63 380 212 319.9 110	212 319.9 0.011 213 320.41 0.011	8 8	151 1	1.01052	
213 320.41 440 214 325.67 780	214 325.67 0.011 215 332.26 0.011	8 8	152 1 153 1	0.870672	*No new flow *No new flow
215 332.26 390	216 343.45 0.011	8	154 1	0.27	*Added-new
216 343.45 400 200 299.4 250	217 355.58 0.011 220 306.55 0.011	8 8	155 1 156 1	0.498168 3.43	*Added-new
220 306.55 430	221 309.67 0.011	8	157 1 160 1	2.43 4.239672	*Added-new
221 309.67 430 222 314.72 460	222 314.72 0.011 223 321.86 0.011	8 8	161 1	2.01	
223 321.86 420	224 323.79 0.011	8	162 1 200 1	2.01 9.888232	
224 323.79 410 225 330.54 400	225 330.54 0.011 226 336.66 0.011	8 8	201 1	3.630424	
226 336.66 380 213 320.41 360	227 343.49 0.011	8	202 1 203 1	2.149016 0.691152	*No new flow
230 321.02 430	230 321.02 0.011 231 327 0.011	8 8	204 1	2.907856	
230 321.02 580 232 322.97 360	232 322.97 0.011 233 323.85 0.011	8 8	205 1 206 1	0.520608	*No new flow
233 323.85 400	234 326.56 0.011	8	207 1 208 1	0.759344	
234 326.56 400 235 334.49 400	235 334.49 0.011 236 341.76 0.011	8 8	209 1	1.280672 0.391328	
236 341.76 170	237 370.9 0.011	8	210 1 211 1	3.271752	
232 322.97 400 238 325.61 400	238 325.61 0.011 239 333.14 0.011	8 8	212 1	0.601392	
239 333.14 400	240 355.65 0.011	8	213 1 214 1	1.148232 4.33164	
240 355.65 170 240 355.65 370	241 379.43 0.011 242 358.93 0.011	8 8	215 1	3.829136	
242 358.93 430	243 383.5 0.011	8	216 1 217 1	4.331792	
SANITARY LOADING			220 1	1.782024	
100 1 101 1	13.54 *Added-new 5.16884		221 1 222 1	2.010544 0.94976	
102 1	3.168888		223 1	2.51	*Added-new
103 1 104 1	2.448016 0.869344		224 1 225 1	3.180272 2.300016	
105 1	0.251328		226 1	1.532	
106 1 107 1	0.638168 0.759344		227 1 230 1	0.88052 0.991848	
108 1	0.498168		231 1 232 1	0.991848	
109 1 110 1	1.81 *Added-new 1.141328		233 1	0.870672	
111 1	1.141328		234 1 235 1	0.870672	
112 1 113 1	1.220064 1.33		236 1	0.74052	
114 1 115 1	2.468384		237 1 238 1	0.5 2.230536	
115 1 116 1	2.068296 1.838168		239 1	2.230536	
117 1 118 1	1.950672		241 1 242 1	1.490016 1.238688	
120 1	0.14 *Added-new 1.140672		243 1	1.238688	
121 1 122 1	0.870672 0.661176		251 1 ENDFILE	0.41	*Added-new
123 1	1.01				
124 1 125 1	3.018168 0.87 *Added-new				
126 1	2.569104				
127 1 128 1	1.801848 1.531848				
129 1 130 1	2.938168				
131 1	0.75 *Added-new 1.417776				
132 1 133 1	1.16 *Added-new				
134 1	1.02 *Added-new 0.68 *Added-new				
135 1 136 1	0.829344 0.708016				
137 1	0.731328				
140 1 141 1	0.498168 1.308168				
142 1	0.908016				
143 1 144 1	0.791328 0.84				
145 1	1.86 *Added-new				
146 1 147 1	1.73 3.58052				

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*NIPOMO CSD SEWER MODEL OF EXISTING SYSTEM, FUTURE FLOWS LS AREA *FBRACKEN.DTA BRACKEN PAGESIZE 84 DESIGN CRITERIA 0.9 15 0.9 21 0.9 999 ANALYSIS CRITERIA 0.9 15 0.9 21 0.9 999 PEAKING 3.0 1 OUTPUT FBRACKEN.OUT UNITS 0 0 1 0 0 0 0 GEOMETRY 336.51 0.011 8 330 333.8 150 331 336.51 60 332 337.6 0.011 8 331 339.46 0.011 8 230 333 332 337.6 332 337.6 80 334 339.24 0.011 8 SANITARY LOADING 4.926 331 1 332 1 0.251328 0.74052 333 1 0.251328 334 1 ENDFILE

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*NIPOMO CSD SEWER MODEL OF EXISTING SYSTEM, FUTURE FLOWS *FNOAKGLN.DTA N. OAKGLEN LS AREA PAGESIZE 84 DESIGN CRITERIA 0.9 15 0.9 21 0.9 999 ANALYSIS CRITERIA 0.9 15 0.9 21 0.9 999 PEAKING 3.0 0.9 OUTPUT FNOAK.OUT UNITS 0 0 1 0 0 0 0 GEOMETRY 163 332.85 140 164 341.3 0.011 8 333.76 0.011 163 332.85 230 165 8 332.85 0.011 222 326.81 100 163 8 165 335.4 0.011 8 333.76 380 166 335.4 310 167 336.95 0.011 8 166 336.95 600 346.48 0.011 167 168 8 SANITARY LOADING 0.251328 164 1 164 1 0.318648 0.498168 165 1 166 1 22.968168 3.94132 167 1 1.261848 168 1

ENDFILE

*NIPOMO	CSD SEW	ER MODEL	OF EX	ISTIN	G SYS	TEM,	FUTURE	FLOW	S			
*FMHPBL/	AK.DTA						BLACK		KE	MHP	LS	AREA
PAGESIZE DESIGN	E 84 CRITERIA	0.9 1	5 0.90	21	0.90	000						
	S CRITER				0.90							
	3.0 0.9											
	FMHPBL.O	100000000										
GEOMETRY	0100	0 0										
300	343.73	60	301	34	9.01	0.01	1 8					
999	334.93	100	300		3.73	0.01			BLACK	LAKE L	s a M	HP
301	349.01	400	302		0.58	0.01						
302 303	350.58	130 300	303		1.22	0.01						
303	351.22 352.72	140	304 305		2.72	0.01						
305	353.55	120	306		4.05	0.01						
306	354.05	230	307	35	6.37	0.01	1 8					
307	356.37	300	308		8.7	0.01						
306 309	354.05	190 100	309 310	35	5.22	0.01						
300	343.73	90	250		5.09	0.01						
250	345.09	150	311	35	0.46	0.01						
*250	345.09	342	251	34	8	0.01	1 8		*NO	SAN. LO	ADING	
311	350.46	10	312		1.08	0.01						
312 313	351.08 367.02	280	313 314		7.02	0.01						
*315	357.02		314		9.17	0.01			*RF	DUNDANT	8	
315	357.02	120	316	35	7.26	0.01				o ono mun		
312	351.08	260	317		2.18	0.01						
317	352.18	100	329		4.98	0.01						
329 327	354.98 356.22	330 150	327 315		6.22	0.01						
327	356.22	470	328		7.22	0.01						
317	352.18	280	320	36	1.13	0.01						
320	361.13	280	321		5.33	0.01						
320	361.13	260	322		7.75	0.01						
322 322	377.75	260 280	323 324		0.93	0.01						
324	379.05	380	325		8.32	0.01						
325	398.32	200	326	40		0.01						
	LOADIN											
301 303	1	0.41 1.02934	1									
303	1	0.74052		*No n	ew fl	OW						
305	1	0.36801		*No n								
306	1	3.04434		*No n	ew fl	OW						
307	1	0.87067		*No n								
308	1	0.74052		*No n								
309 310	i	0.49816		*No n *No n								
311	i	0.61934		*No n								
313	1	1.61119	2	*No n								
314	1	0.99184		*No n								
315 316	1	0.87067		*No n								
317	1	0.87067		*No n								
320	i	0.87067		*No n								
321	1	0.87067		*No n								
322	1	0.87067		*No n								
323 324	1	0.74052		*No n								
325	1	1.64868		no n	CH TI	UW						
326	i	0.82934										
327	1	1.28067										
328	1	1.44868	8	***	1000							
329 ENDFILE	1	0.41		*Adde	d-nev							
CHUFILE												

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*NIPOMO CSD SEWER MODEL OF EXISTING SYSTEM, FUTURE FLOWS GARDENIA LS AREA *FGARDENA.DTA PAGESIZE 84 DESIGN CRITERIA 0.9 15 0.90 21 0.90 999 ANALYSIS CRITERIA 0.9 15 0.90 21 0.90 999 PEAKING 3.0 0.9 OUTPUT FGARDEN.OUT UNITS 0 0 1 0 0 0 0 GEOMETRY 169 170 361.5 0.11 338.6 430 8 361.5 180 375.52 0.11 8 170 171 362.76 0.11 170 361.5 220 172 8 172 362.76 270 173 363.44 0.11 8 172 362.76 280 174 363.48 0.11 8 SANITARY LOADING 4.877 170 1 0.74052 *No new flow 171 1 172 1 1.328168 173 1 2.06 1.491328 174 1 ENDFILE

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APPENDIX C

Hydrant Tests/Calibration Results

FIREDATA.XLS

NIPOMO CSD Nipomo CSD Water and Sewer Master Plan VT-N04-100-01, jal/cmf 7-18-95 firedata.xls Hydrant Flow Test Results Used to Calibrate the Existing Water Model

TEST LOCATION		FIELD MEASUREMENTS			MODELED RESULTS		DIFFERENCE		COMMENT	
Мар	Node No. at Flowing		Static	Flow	Residual	Static	Residual	Static	Residual	
	Hydrant		(psi)	(gpm)	(psi)	(psi)	(psi)	(psi)	(psi)	
nitlal Ru	ns:									
1	(1)	(1)	72	1,330	62	(1)	(1)			Request re-test
2	(1)	(1)	95	1,560	70	(1)	(1)			Request re-test
3	(1)	(1)	88	1,430	58	(1)	(1)			Request re-test
4	(1)	(1)	76	1,150	38	(1)	(1)			Request re-test
5	(1)	(1)	90	1,088	34	(1)	(1)			Request re-test
6	700	701	85	1,088	60	88	73	3	13	Request re-test
7	137	702	65	1,150	40	60	46	-5	6	Request re-test
8	322	323	68	1,180	47	56	39	-12	-8	Request re-test
9	143	703	70	1,180	53	67	55	-3	2	Good run
									-	Modeled static low; concurs
10	362	361	82	1,055	60	70	58	-12	-2	with measured hydrant flow
11	203	204	93	1,430	74	87	76	-6	2	Modeled static slightly low
								1000	1122	Modeled static low; concurs
12	167	166	105	1,460	83	93	81	-12	-2	with measured hydrant flow Modeled static low; concurs
13	215	216	90	1,360	70	79	69	-11	-1	with measured hydrant flow Modeled static low; concurs
14	410	410	50	932	32	43	31	-7	-1	with measured hydrant flow Modeled static low; concurs
15	408	704	56	834	32	48	34	-8	2	with measured hydrant flow
ydrant F	Re-Tests:									
1	236	228	80	1,237	67	87	51	7	-16	Checked modeling input. No evident modeling problems.
2		274	91	1,500	76	94	20 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	3	2	Good run
3		108	88	1,320	69	91		3	1	Good run
4		330	80	1,320	56	80	2.2013	0	4	
4	1 (10,5 (17) A.)	293	STS (7)		1 m m m m m m m m m m m m m m m m m m m	1.	8 (S16)	2	4	Good run
5	295	293	92	1,022	44	94	4/	2	3	Good run Checked modeling input. No
6	132	701	85	1,237	55	90) 71	5	16	evident modeling problems. Adjust "C' values of pipes in
7	137	321	60	1,150	40	62	. 47	2	7	vicinity Adjust "C' values of pipes in
8	329	702	70	1,022	40	61	48	-9	8	vicinity

(1) - Hydrants tested with residual taken at same hydrant as flow recorded, disregard.

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